FDS



History of Construction

For Compliance with the EPA Coal Combustion Residuals (CCR) Rule 40 CFR §257.73(c)

Former Erickson Power Station – Former Forebay, Former Retention Basin, and Former Clear Water Pond August 8, 2025

Prepared for: Lansing Board of Water & Light Former Erickson Power Station 3725 South Canal Road Lansing, Michigan 48917

Prepared by: HDR MICHIGAN, Inc. 1000 Oakbrook Drive, Suite 200 Ann Arbor, Michigan 48104



Contents

1	Introd	luction	3				
	1.1	Site Location	3				
	1.2	Site Description	4				
2	Histo	ry of Construction Requirements	5				
3	Histo	ry of Construction	6				
	3.1	§257.73 (c)(1)(i) - Owner and Unit Identification	6				
	3.2	§257.73 (c)(1)(ii) - Unit Location on USGS Quadrangle	6				
	3.3	§257.73 (c)(1)(iii) - Purpose of the CCR Unit	7				
	3.4	§257.73 (c)(1)(iv) – Watershed Information	8				
	3.5	§257.73 (c)(1)(v) - Foundation and Abutment Materials	8				
		3.5.1 Physical Properties					
	3.6	§257.73 (c)(1)(vi) - Construction, Description of the Materials, Methods, and Timeframe of Construction	12				
	3.7	§257.73 (c)(1)(vii) – Drawings	13				
	3.8	§257.73 (c)(1)(viii) - Instrumentation	13				
	3.9 §257.73 (c)(1)(ix) - Area Capacity Data						
	3.10 §257.73 (c)(1)(x) - Spillway and Diversion Design Features						
	3.11	§257.73 (c)(1)(xi) - Construction Specifications and Provisions for Operations and Maintenance	15				
	3.12	§257.73 (c)(1)(xii) - Record of Structural Instability	15				
4	Refer	ences	15				
5	Attac	hments	16				
		Tables					
Table	2-1. L	_ist of History of Construction Requirements	6				
		List of Available Borings, Test Pits, Monitoring Wells					
		Figures					
		Figures					
•		te Vicinity Map					
_		rickson Power Station Site Configuration					
_		arrier Creek Drainage Basin					
Figure	e 4. A _l	pproximate Boring/Monitoring Well Locations	10				



This page is intentionally left blank.



1 Introduction

HDR MICHIGAN, Inc. (HDR) has prepared this revised History of Construction for the Former Forebay, Former Retention Basin, and Former Clear Water Pond at the Former Erickson Power Station following the requirements of the Federal Coal Combustion Residuals (CCR) Rule to demonstrate compliance of the Former Erickson Power Station in Lansing, Michigan.

On April 17, 2015, the United States Environmental Protection Agency (EPA) issued the final rule (Ref. [1]) for disposal of Coal Combustion Residuals (CCR) under Subtitle D of the Resource Conservation and Recovery Act (RCRA). CCR Rule 40 CFR §257.73(b) requires that owners or operators of an existing CCR surface impoundment that either 1) has a height of five feet or more and a storage volume of 20 acre-feet or more; or 2) has a height of 20 feet or more compile a history of construction, which shall contain, to the extent feasible, the information specified in 40 CFR §257.73(c)(1)(i) through (xii). It was previously determined that the Former Forebay, Former Retention Basin, and Former Clear Water Pond at the Former Erickson Power Station met the first criteria with heights of five feet or more and storage volumes greater than 20 acre-feet.

The revised History of Construction report presented herein addresses the specific requirements of 40 CFR §257.73(c)(1)(i) through (xii). If there is any significant change to any information compiled under paragraph 40 CFR §257.73(c)(1), the owner or operator of the CCR unit must update the relevant information and place it in the facility's operating record as required by 40 CFR §257.105(f)(9).

This History of Construction was prepared by Mr. Bryce Burkett, P.E., and was reviewed in accordance with HDR's internal review policy by Mr. Andrew Bertapelle, P.E., both of HDR. Mr. Burkett is a registered Professional Engineer in the State of Michigan.

1.1 Site Location

The Former Erickson Power Station was an electrical power generation facility located at 3725 South Canal Road, Lansing, Michigan which is owned and operated by Lansing Board of Water & Light (BWL). The latitude and longitude of the Erickson Power Station are approximately 42.692422 N and 84.657764 W. The site is located southwest of Lansing, Michigan, near the intersection of Interstates 69 and 96, as shown in the site vicinity map, Figure 1.

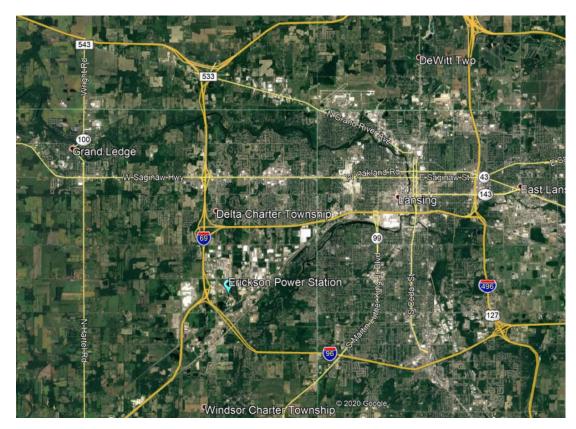


Figure 1. Site Vicinity Map

1.2 Site Description

The Former Erickson Power Station was constructed starting in 1970 and completed in 1973. The Former Station contained a single coal-fired steam turbine/generator capable of producing 165 megawatts of electricity, while it was still in operation. Coal-fired operations at the Former Station and CCR process water discharges ceased in 2022 as part of BWL's move to cleaner energy sources. Closure of the three (3) former regulated CCR surface impoundments began in February 2023. Since then, the former regulated CCR units have been physically closed, and all CCR materials have been removed and appropriately managed. The Former Forebay and Former Retention Basin were then filled with clean fill material and all former impoundments were graded to direct stormwater runoff to the Former Impoundment area. Verification of CCR removal from the regulated former CCR units was completed and documented in the CCR Removal Report, dated November 4, 2024 (Ref. [5]).

Following the decommissioning of the three (3) regulated CCR surface impoundments, the entire impoundment system (including the Former Impoundment) now collectively functions as a limited stormwater collection basin. These former impoundments form a roughly contiguous drainage system. Their only inflow is stormwater from direct rainfall onto the impoundment system.

Figure 2 displays the Former Erickson Power Station site configuration.





Figure 2. Erickson Power Station Site Configuration

2 History of Construction Requirements

The requirements to be included in the History of Construction Report for existing CCR surface impoundments are detailed in 40 CFR §257.73: Structural integrity criteria for existing CCR surface impoundments. CCR Rule 40 CFR §257.73(c) states that the history of construction for an existing CCR impoundment (i.e. Former Forebay, Former Retention Basin, and Former Clear Water Pond) is to be compiled and contain the information specified in 40 CFR §257.73(c)(1)(i) through (xii). Table 2-1 summarizes the information from paragraphs 40 CFR §257.73(c)(1)(i) through (xii), as well as the location of the information presented in this document.



Table 2-1. List of History of Construction Requirements

40 CFR Rule	Rule Information	Document Section
§257.73 (c)(1)(i)	Owner/Unit Information	Section 3.1
§257.73 (c)(1)(ii)	USGS Map Location	Section 3.2
§257.73 (c)(1)(iii)	Purpose of CCR Unit	Section 3.3
§257.73 (c)(1)(iv)	Name and Size of Watershed	Section 3.4
§257.73 (c)(1)(v)	Description of Foundation and Abutment Materials	Section 3.5
§257.73 (c)(1)(vi)	Statement of Materials Used in Construction, Method of Site Preparation, Dates of Construction	Section 3.6
§257.73 (c)(1)(vii)	Detailed Drawings of Unit	Section 3.7
§257.73 (c)(1)(viii)	Existing Instrumentation Details	Section 3.8
§257.73 (c)(1)(ix)	Area-Capacity Curves	Section 3.9
§257.73 (c)(1)(x)	Spillway and Diversion Design Features	Section 3.10
§257.73 (c)(1)(xi)	Construction Specifications and Surveillance, Maintenance, and Repair Provisions	Section 3.11
§257.73 (c)(1)(xii)	Structural Instability Records	Section 3.12

3 History of Construction

3.1 §257.73 (c)(1)(i) - Owner and Unit Identification

§257.73 (c)(1)(i): The name and address of the person(s) owning or operating the CCR unit; the name associated with the CCR unit; and the identification number of the CCR unit if one has been assigned by the state.

The Former Erickson Power Station was an electrical power generation facility located at 3725 South Canal Road, Lansing, Michigan which is owned and operated by Lansing Board of Water & Light (BWL).

The names associated with the former CCR units are the Former Forebay, Former Retention Basin, and Former Clear Water Pond.

The units have not been assigned identification numbers by the State of Michigan.

3.2 §257.73 (c)(1)(ii) - Unit Location on USGS Quadrangle

§257.73 (c)(1)(ii): The location of the CCR unit identified on the most recent U.S. Geological Survey (USGS) 7 $\frac{1}{2}$ minute or 15 minute topographic quadrangle map, or a topographic map of equivalent scale if a USGS map is not available.

Attachment 1 presents the *Site Location Map* with the Dimondale Quadrangle, Michigan, Eaton County, 7.5-minute series USGS Quadrangle, dated 2023. The locations of the Former Forebay, Former Retention Basin, and Former Clear Water Pond are shown on the quadrangle.



3.3 §257.73 (c)(1)(iii) - Purpose of the CCR Unit

§257.73 (c)(1)(iii): A statement of the purpose for which the CCR unit is being used.

The Former Erickson Power Station was constructed starting in 1970 and completed in 1973. During active operations, the Former Station contained a single coal-fired steam turbine/generator capable of producing 165 megawatts of electricity and CCR was stored in dewatering tanks (former hydro-bins). After the majority of the CCR was removed from the waste stream at the former hydro-bins, flow was discharged into three CCR impoundments in sequence: the Former Forebay, Former Retention Basin, and Former Clear Water Pond.

The Former Station ceased coal-fired power generation operations in November 2022. In February 2023, closure of the Former Forebay, Former Retention Basin, and Former Clear Water Pond began. Since then, the former regulated CCR units have been physically closed and all CCR materials have been removed and appropriately managed. The Former Forebay and Former Retention Basin were then filled with clean fill material and all former impoundments were graded to direct stormwater runoff to the Former Impoundment area.

Verification of CCR removal from the regulated former CCR units was completed and documented in the CCR Removal Report (Ref. [5]).

The locations of the former conveyances through the former impoundment system can be found on the Mayotte Design & Engineering Drawings (MD&E) (Ref. [13]), provided in Attachment 4. Additional description of these conveyances is also available in the previous History of Construction reports (Ref. [7] and Ref. [8]) for the Former Station. Current and historical grading, as well as locations and elevations of former impoundment system features, may also be found in the HDR Ash Impoundments Closure Drawings (Ref. [6]).

During decommissioning of the Former Forebay, Former Retention Basin, and Former Clear Water Pond, all hydraulic conveyance structures (e.g. inlet and outlet piping) were cut back and/or removed, except for the Emergency Overflow Structure at the Former Clear Water Pond. This outfall structure is located on the northeast corner of the Former Clear Water Pond and discharges to a swale that flows north and east and eventually directs flow to Carrier Creek and then to the Grand River. This structure was previously comprised of a horizontal outfall pipe and a vertical steel standpipe. During decommissioning of the former impoundment system, the vertical standpipe was removed and only the horizontal outfall pipe remains, with an invert elevation of 875.3 feet North American Vertical Datum of 1988 (NAVD 88).

The berm formerly separating the Former Impoundment and the Former Clear Water Pond was also removed during system decommissioning, allowing the Former Clear Water Pond Emergency Overflow Structure to serve as the sole outfall serving the entire former impoundment system. However, hydrologic modelling shows that this outfall would not spill over in a 100-year flood event (Ref. [9]). Additionally, to the best of BWL's knowledge the Emergency Overflow Structure was never utilized, even prior to system decommissioning.

Following decommissioning, the entire former impoundment system (including the Former Impoundment) collectively functions as a limited stormwater collection basin. These former impoundments form a roughly contiguous drainage system. Their only inflow is stormwater from direct rainfall onto the impoundment system.



3.4 §257.73 (c)(1)(iv) – Watershed Information

§257.73 (c)(1)(iv): The name and size in acres of the watershed within which the CCR unit is located.

According to the EPA WATERS GeoViewer (Ref. [2]), the Former Forebay, Former Retention Pond, and Former Clear Water Pond impoundments are located within the Carrier Creek-Grand River subwatershed, which has a size of approximately 22,700 acres. The Former Erickson Power Station is part of the Carrier Creek drainage basin shown in Figure 3.

No natural drainage runs into the Former Forebay, Former Retention Basin, or Former Clear Water Pond. The drainage areas of the Former Forebay, Former Retention Basin, and Former Clear Water Pond are approximately 2.76 acres, 3.73 acres, and 5.74 acres, respectively.



Figure 3. Carrier Creek Drainage Basin

3.5 §257.73 (c)(1)(v) - Foundation and Abutment Materials

§257.73 (c)(1)(v): A description of the physical and engineering properties of the foundation and abutment materials on which the CCR unit is constructed.

Surficial soils in the area of the Former Forebay, Former Retention Basin, and Former Clear Water Pond are shown to be composed of medium-textured glacial till on the Quaternary Geology of Southern Michigan Map (1982). Glacial till is typically a dense, heterogeneous mixture of soil ranging from clay to cobbles or boulders. Additionally, the map shows that glacial outwash and postglacial alluvium are present close to the site, which is typically comprised of sand or alternating layers of small gravel to heavy cobbles. These soils form the foundations of the Former Forebay, Former Retention Basin, and Former Clear Water Pond. The Former Forebay, Former Retention Basin, and Former



Clear Water Pond were constructed entirely with perimeter embankments, therefore there were no abutments.

Prior to the construction of the former impoundment system, a subsurface investigation program was performed in 1969 by Dames & Moore. The soil boring logs performed for that study are presented in the Location Restrictions Report prepared by Mayotte Design & Engineering (MD&E) (Ref. [12]). In addition to the 1969 soil borings, test pits were performed at the site by MD&E in 2018. In 2018, SME performed three soil borings to the west of the Former Forebay and Former Retention Basin for the new gas-fired combustion turbine power plant for BWL (Ref. [15]). From 2019 to 2025, HDR installed 42 wells at 21 distinct locations across the site. Monitoring wells MW-3 and MW-4 were installed in the vicinity of the Former Forebay and the Former Retention Basin, respectively, and MW-1 and MW-14 were both installed in the vicinity of the Former Clear Water Pond (Ref. [5]).

Table 3-1 details the borings, test pits, and monitoring wells which were reviewed for the physical and engineering properties of the foundation material of the Former Forebay, Former Retention Basin, and Former Clear Water Pond.

Table 3-1. List of Available Borings, Test Pits, Monitoring Wells

ID	Туре	Year	Engineering Firm	Reference
AP-3 to AP-6	Geotechnical Borings	1969	Dames & Moore	Ref. [12]
AP-2	Test Pit	1969	Dames & Moore	Ref. [12]
ECT-18-B01 thru ECT-18-B03	Geotechnical Borings	2018	SME	Ref. [15]
CW-SB-01 thru CW- SB-03	Geotechnical Borings	2018	MD&E	Ref. [12]
EW-F-1 thru EW-F-6	Test Pits	2018	MD&E	Ref. [12]
MW-1, MW-3, MW-4, MW-14	Monitoring Wells	2019-2023	HDR	Ref. [5]

The approximate boring, test pit, and monitoring well locations are shown on . The borings logs, test pit records, and monitoring well logs are provided in Attachment 2.



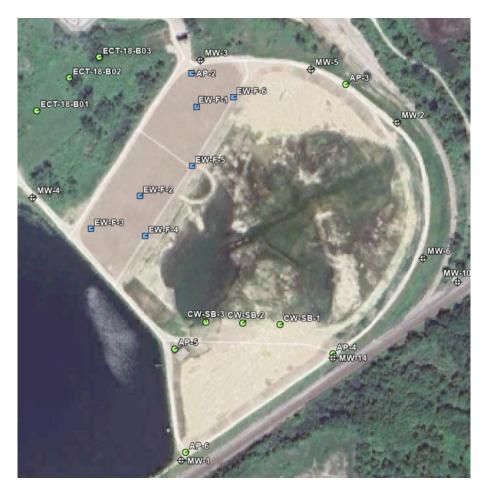


Figure 4. Approximate Boring/Monitoring Well Locations

The physical and engineering properties of the embankment and foundation materials are described in Sections 3.5.1 and 3.5.2.

3.5.1 Physical Properties

The boring logs, test pit records, and monitoring well logs from subsurface investigations (listed in Table 3-1) indicate that the foundations of the Former Forebay, Former Retention Basin, and Former Clear Water Pond are composed primarily of alternating layers of cohesive and granular soils. These include lean clay, sandy clay, clayey sand, silty sand, sand, silt, silty sand, and clayey silt. Gravel, shale fragments, and limestone fragments were observed in these interbedded layers. Sandstone was encountered at the bottom of the deepest boring (AP-5), at El. 810.4 feet NAVD 88, approximately 60 feet below grade.

The foundations of the Former Forebay and Former Retention Basin embankments were cut to approximately El. 870.9 feet NAVD 88 prior to construction of the embankments. There are no records of borings through the embankments of the Former Forebay or Former Retention Basin. However, the installation logs of MW-1 and MW-14 indicate that the embankment of the Former Clear Water Pond is comprised of firm to stiff cohesive material (sandy lean clay). The installation log for MW-1 also indicated the presence of gravel in the embankment material.



Laboratory test results were available for samples taken from Borings ECT-18-B01 through ECT-18-B03, which were performed outside of the footprint of the former impoundments, but in the vicinity of the site (i.e. approximately 300 feet northwest of the former impoundments). Laboratory test results were available for the subsurface foundation material (i.e. below El. 870.9 feet NAVD 88). Undrained shear strengths obtained from field estimates with a hand penetrometer or torvane in the cohesive soils ranged from 1,000 psf (stiff) to greater than 4,500 psf (very stiff). Moisture contents in the cohesive soils ranged between 7 and 13 percent. SPT blow counts indicated that the granular soils ranged from very loose to very dense, with blow counts ranging from 3 to greater than 50 blows per foot. There were no laboratory test results presented on the available boring logs for the Former Clear Water Pond.

3.5.2 Engineering Properties

Engineering properties for the foundation materials assumed for the original design of the Former Forebay, Former Retention Basin, and Former Clear Water Pond are not available. However, field investigations using Standard Penetration Tests (SPTs) provide insight into the properties of the foundation soils.

SPTs were performed at four borings (ECT-18-B01 through ECT-18-B03 and AP-3) in the vicinity of the Former Forebay and Former Retention Basin. These borings included blow counts (N-values) for the foundation materials but were located outside the footprints of the Former Forebay and Former Retention Basin.

The N-values typically ranged from 5 to 20 blows per foot (bpf), from approximately El. 871.5 feet to approximately El. 866 feet, with shear strength values ranging from 1,000 psf to greater than 4,500 psf, as measured in the field with a penetrometer or torvane, indicating stiff to hard cohesive soils (sandy lean clay and lean clay). Underlying the stiff to very stiff cohesive soils, very loose to medium-dense granular soils (clayey sand and some silt), with N-values ranging from 3 to 30 bpf, were encountered to approximately El. 854 feet. Cohesive soils consisting of stiff to very stiff sandy lean clay were observed interbedding the granular soils in some of the borings. Underlying the very loose to medium-dense granular soils, stiff to hard cohesive soils (sandy lean clay) were encountered to approximately El. 850 feet with N-values ranging from 6 to 34 bpf and shear strength values of greater than 4,500 psf, indicating stiff to hard cohesive soils. Below this zone, medium-dense to very dense granular soils were encountered with N-values ranging from 15 to greater than 50 bpf to El. 811 feet, which is where sandstone was encountered. Sandstone was encountered in boring AP-5 (the deepest boring performed) and the boring was ultimately terminated after refusal from the SPT.

SPTs were also performed at three borings (AP-4 through AP-6) in the vicinity of the Former Clear Water Pond, including N-values of the foundation material. The existing ground surface at the time of the field exploration ranged from approximately El. 871 to 873 feet.

The N-values typically ranged from 2 to 7, from the existing ground surface (prior to construction of the embankment) to approximately El. 855, indicating loose granular soils. Underlying the loose granular soils, medium-dense granular soils with N-values ranging from 10 to 27 were encountered to approximately El. 825 to El. 820, where a dense granular layer with an N-value of 47 was encountered. Below the dense granular layer,



medium-dense granular soils were encountered with N-values ranging from 16 to 25 to El. 810 feet, which is where sandstone was encountered, and the boring was ultimately terminated after refusal from the SPT.

HDR is not aware of available data that would allow interpretation of the engineering properties of the embankment soils of the Former Clear Water Pond, other than GZA 2012 (Ref. [3]), which referenced the original specifications for the embankment, and noted that the natural ground surface, which also forms the liner, was stripped and scarified to provide a bond with the first layer of dike fill. The embankment was constructed primarily with selected on-site clay borrow and placed/compacted under controlled conditions.

The boring logs, along with recorded SPT blow counts, performed in the vicinity of the Former Forebay, Former Retention Basin, and Former Clear Water Pond are presented in Attachment 2. For additional discussion of the engineering properties of the embankment and foundation soils, refer to the HDR Initial Structural Stability and Safety Factor Assessment Report (Ref. [10]).

3.6 §257.73 (c)(1)(vi) - Construction, Description of the Materials, Methods, and Timeframe of Construction

§257.73 (c)(1)(vi): A statement of the type, size, range, and physical and engineering properties of the materials used in constructing each zone or stage of the CCR unit; the method of site preparation and construction of each zone of the CCR unit; and the approximate dates of construction of each successive stage of construction of the CCR unit.

The Former Clear Water Pond was constructed between 1970 and 1973 as part of the original construction of the former impoundment system for the Former Erickson Power Station, for the purpose of storing process water prior to return to the Former Station through the Pump House. The Pump House is located on the northwest side of the Former Clear Water Pond. Construction drawings from 1970 are provided in Attachment 3, and grading profiles from 2018 are provided in Attachment 5. A review of the installation logs of MW-1 and MW-14 indicates that the Former Clear Water Pond embankment generally consists of firm to stiff sandy lean clay. No laboratory tests or construction records were available to confirm the strength or placement methods, other than the reference to the original construction specifications in GZA 2012 (Ref. [3]). A review of the available records and discussions with BWL staff indicate that there were no major modifications made to the Former Clear Water Pond between the original construction and the decommissioning of the former impoundment system.

The Former Forebay and Former Retention Basin were constructed in 2014. Details of the construction procedures and construction materials, as summarized below, can be found in the Construction Documentation Report prepared by Mayotte Design & Engineering, P.C. (May 2015) (Ref. [13]). Construction Drawings and As-Built Drawings are presented in Attachment 4 and Attachment 6 of this report, respectively. Further details of the 2014 former impoundment system reconfiguration can also be found in previous versions of the site History of Construction reports (Ref. [7] and Ref. [8]).

Following the end of coal-fired activities at the Former Station in 2022, the Former Forebay, Former Retention Basin, and Former Clear Water Pond were decommissioned via removal



of coal combustion materials. Closure of these former regulated CCR units began in February 2023. Verification of CCR removal from the regulated former CCR units was completed and documented in the CCR Removal Report (Ref. [5]).

Following excavation, the Former Forebay and Former Retention Basin were filled with clean fill material and all former impoundments were graded to direct stormwater runoff to the Former Impoundment area. The entire former impoundment system area now functions only as a limited stormwater collection basin. These former impoundments form a roughly contiguous drainage system and are no longer connected. Their only inflow is stormwater from direct rainfall onto the former impoundment system. The berm separating the Former Clear Water Pont and the Former Impoundment was also removed. The only outfall serving the former impoundment system is now the Emergency Outfall Structure at the Former Clear Water Pond, which has been modified such that only the horizontal outlet pipe remains, with an invert elevation of El. 875.3 ft NAVD88.

2025 drawings detailing conditions following decommissioning of the former impoundment system are also available in HDR's Ash Impoundments Closure Drawings (Ref. [6]).

3.7 §257.73 (c)(1)(vii) – Drawings

§257.73 (c)(1)(vii): At a scale that details engineering structures and appurtenances relevant to the design, construction, operation, and maintenance of the CCR unit, detailed dimensional drawings of the CCR unit, including a plan view and cross sections of the length and width of the CCR unit, showing all zones, foundation improvements, drainage provisions, spillways, diversion ditches, outlets, instrument locations, and slope protection, in addition to the normal operating pool surface elevation and the maximum pool surface elevation following peak discharge from the inflow design flood, the expected maximum depth of CCR within the CCR surface impoundment, and any identifiable natural or manmade features that could adversely affect operation of the CCR unit due to malfunction or mis-operation.

Available construction drawings from 1970, provided by BWL, are presented in Attachment 3. Additionally, grading profiles, along with a plan view locating the sections, developed by NTH Consultants, Ltd. (Ref. [14]), are provided in Attachment 5. The topographic survey used in the development of the grading plans were collected in 2018 by Droneview.

2014 construction drawings prepared by MD&E (Ref. [13]), provided by BWL, are presented in Attachment 4, along with plan views and cross-sectional views of the Former Forebay and Former Retention Basin. As-built drawings are presented in Attachment 6.

2025 drawings detailing conditions following decommissioning of the former impoundment system are also available in HDR's Ash Impoundments Closure Drawings (Ref. [6]).

3.8 §257.73 (c)(1)(viii) - Instrumentation

§257.73 (c)(1)(viii): A description of the type, purpose, and location of existing instrumentation.

In 2019 and 2020, HDR installed six monitoring wells for the Former Erickson Power Station as part of the Hydrogeologic Characterization of the site to monitor the groundwater across the Former Erickson Power Station impoundment system (Ref. [5]). MW-3 and



MW-4 were installed in the vicinity of the Former Forebay and Former Retention Basin, respectively, and MW-1 and MW-14 were installed in the vicinity of the Former Clear Water Pond. The locations of these wells are shown in Figure 4. The installation logs of MW-1, MW-3, MW-4, and MW-14 are provided in Attachment 2.

Two temporary piezometers, designated as RBPZ-1 and RBPZ-2, were installed on March 10, 2023, by SME in the embankment that separates the Retention Basin from Lake Delta. The purpose of the temporary piezometer installation was to verify the previous assumptions regarding ground water level and assumed stratigraphy used in seepage and stability analyses for the CCR removal activities. Using the ground water levels obtained from the two temporary piezometers, the stability of the embankments was monitored during construction and remained at low levels indicating stable embankments. The temporary piezometers were monitored throughout construction and abandoned once the Retention Basin was filled with soil and no further monitoring was required.

3.9 §257.73 (c)(1)(ix) - Area Capacity Data

§257.73 (c)(1)(ix): Area-capacity curves for the CCR unit.

Area capacity curves for the former impoundment system – including the Former Forebay, Former Retention Basin, and Former Clear Water Pond – were developed by HDR and are included in the Inflow Design Flood Control System Plan Report (Ref. [9]). See Attachment 8 for capacity calculations.

§257.73 (c)(1)(x) - Spillway and Diversion Design 3.10 **Features**

§257.73 (c)(1)(x): A description of each spillway and diversion design features and capacities and calculations used in their determination.

The former regulated CCR surface impoundments at the Former Station have been decommissioned. All effluent hydraulic structures from the Former Forebay and Former Retention Basin were removed, and these former units were filled with clean fill material and graded to direct all runoff to the Former Impoundment area.

The Former Clear Water Pond was also decommissioned and the only remaining outfall from this former unit is the Emergency Overflow Structure located between the Former Clear Water Pond and the swale adjacent to the property line and Canadian National Railroad right-of way. This structure was previously comprised of a horizontal outfall pipe and a vertical steel riser pipe. During decommissioning, the vertical riser pipe was removed and only the horizontal outfall pipe remains, with an invert elevation of 875.3 ft NAVD88.

The berm previously separating the Former Clear Water Pond and the Former Impoundment was also removed, and the Emergency Overflow Structure now serves as the sole outfall structure serving the entire former impoundment system. However, hydrologic modelling shows that this outfall would not spill over in a 100-year flood event (Ref. [9]).



3.11 §257.73 (c)(1)(xi) - Construction Specifications and Provisions for Operations and Maintenance

§257.73 (c)(1)(xi): The construction specifications and provisions for surveillance, maintenance, and repair of the CCR unit.

The construction specifications for the Former Forebay and Former Retention Basin are included in the Construction Documentation Report prepared by MD&E (Ref. [13]) and are also presented in Attachment 7. Construction specifications for the Former Clear Water Pond are not available. As noted above, GZA 2012 (Ref. [3]) references the original constructions and presumably had the opportunity to review them.

Prior to the removal of CCR from the former regulated CCR units, BWL performed weekly inspections for the entire former CCR impoundment system, per the requirements of 40 CFR §257.83(a)(1). A typical Weekly Inspection Report is provided in Attachment 9.Following verification of CCR removal (Ref. [5]), and subsequent EGLE approval on November 8, 2024, operating criteria and inspection requirements of 40 CFR §257.83 no longer apply to the former impoundments. However, BWL continues to conduct maintenance on an as-needed basis. BWL also continues to perform corrective action for groundwater, per the post-closure care requirements of 40 CFR §257.83(c)(2).

3.12 §257.73 (c)(1)(xii) - Record of Structural Instability

§257.73 (c)(1)(xii): Any record or knowledge of structural instability of the CCR unit.

Prior to the removal of CCR from the former regulated CCR units, BWL performed weekly inspections for the entire CCR impoundment system. The weekly inspections were completed by qualified individuals to check for potentially hazardous conditions or structural weakness and the results of the inspections are documented internally on Weekly Inspection Reports. As discussed in Section 3.11, above, these weekly inspection requirements are no longer applicable to the former impoundment system, following the verification of CCR removal (Ref. [5]).

An inspection of the Former Clear Water Pond was performed by GZA, referred to as a Round 10 Dam Assessment, at the facility (Ref. [3]). An additional inspection of the Former Clear Water Pond was performed in 2009 by Inspecsol Engineering, Inc. as noted in GZA 2012 (Ref. [3]), however, that report was not available for review.

HDR has also performed annual inspections of the Former Forebay, Former Retention Basin, and Former Clear Water Pond annually since 2020. The results of these inspections are submitted under separate cover, the most recent of which is dated February 20, 2025 (Ref. [4]).

4 References

Ref. [1] Environmental Protection Agency, 40 CFR Parts §257 and §261; Hazardous and Solid Waste Management System; Disposal of Coal Combustion Residuals from Electric Utilities; Final Rule, Washington D.C., April 2015.



Ref. [2]	Environmental Protection Agency, WATERS GeoViewer (2020). https://www.epa.gov/waterdata/waters-geoviewer
Ref. [3]	GZA GeoEnvironmental, Inc. Draft Round 10 Dam Assessment Report, Lansing Board of Water & Light, Erickson Station, Ash Pond, April 30, 2012.
Ref. [4]	HDR Michigan, Inc. Annual Inspection Report - 2025 – Forebay, Retention Basin, and Clear Water Pond, Lansing Board of Water & Light Erickson Power Station, Lansing, Michigan, February 20, 2025.
Ref. [5]	HDR Michigan, Inc. CCR Removal Report, Forebay, Retention Basin, & Clear Water Pond, Lansing Board of Water & Light, Lansing, Michigan, November 4, 2024.
Ref. [6]	HDR Michigan, Inc. Former Erickson Power Station Ash Impoundments Closure Drawings, As-Built, Lansing Board of Water & Light Erickson Power Station, Lansing, Michigan, July 9, 2025.
Ref. [7]	HDR Michigan, Inc. History of Construction, Erickson Power Station – Clear Water Pond, Lansing Board of Water & Light, Lansing, Michigan, June 12, 2020.
Ref. [8]	HDR Michigan, Inc. History of Construction, Erickson Power Station – Forebay and Retention Basin, Lansing Board of Water & Light, Lansing, Michigan, August 10, 2020.
Ref. [9]	HDR Michigan, Inc. Inflow Design Flood Control System Plan, Former Erickson Power Station – Former CCR Surface Impoundments, Lansing Board of Water & Light, Lansing, Michigan, June 6, 2025.
Ref. [10]	HDR Michigan, Inc. Initial Structural Stability and Safety Factor Assessment, Erickson Power Station – CCR Surface Impoundments, Lansing Board of Water & Light, Lansing, Michigan, August 10, 2020.
Ref. [11]	HDR Michigan, Inc. Monitoring Wall Installation Report, Lansing Board of Water & Light Erickson Power Station, Lansing, Michigan, May 15, 2025.
Ref. [12]	Mayotte Design & Engineering, P.C. Compliance with 40CFR257-Locations Restrictions. Lansing Board of Water & Light Erickson Station. October 10, 2018.
Ref. [13]	Mayotte Design & Engineering, P.C. Construction Documentation Report Ash Impoundment System Reconfiguration, Lansing Board of Water & Light Erickson Station, Lansing, Michigan, May 2015.
Ref. [14]	NTH Consultants, Ltd. Closure Plan, CCR Surface Impoundment System, Erickson Power Station, August 16, 2019.
Ref. [15]	SME. Geotechnical Data Report, Lansing Board of Water & Light, New Gas Combined Cycle Plant, Delta Township, Michigan. August 16, 2018.

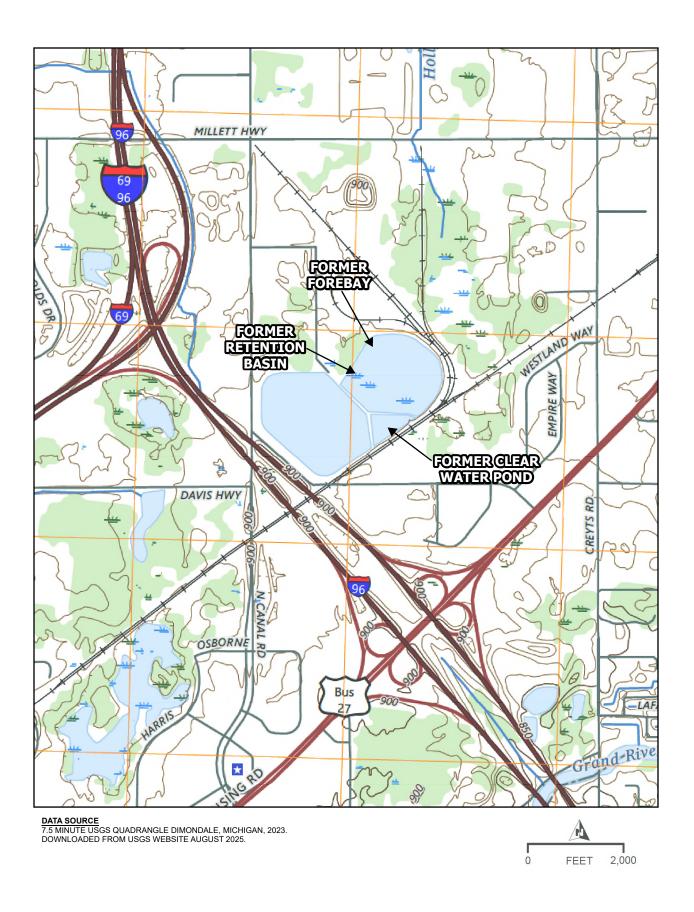
5 Attachments

Attachment 1	Site Location Map
Attachment 2	Boring Logs and Monitoring Well Logs
Attachment 3	1970 Construction Drawings
Attachment 4	Construction Drawings for Former Forebay & Former Retention Basin

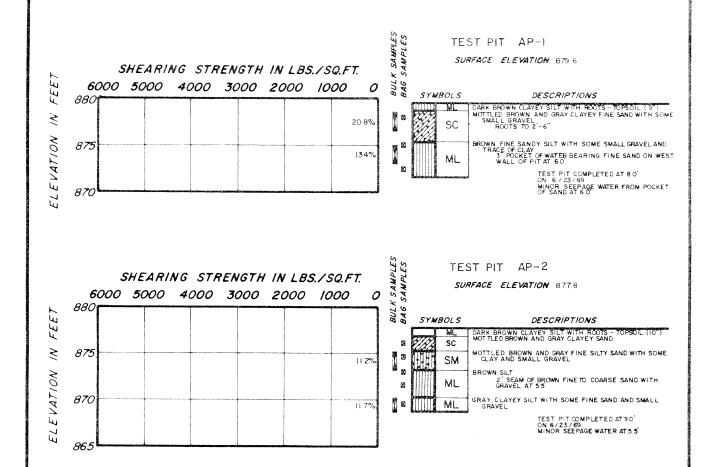


Attachment 5	2018 Grading Profiles
Attachment 6	As-Built Drawings for Former Forebay & Former Retention Basin
Attachment 7	Construction Specifications for Former Forebay & Former Retention Basin
Attachment 8	2025 As-Built Drawings for Impoundment Closure
Attachment 9	2025 Capacity Calculations for Former Impoundment System
Attachment 10	Typical BWL Weekly Inspection Report

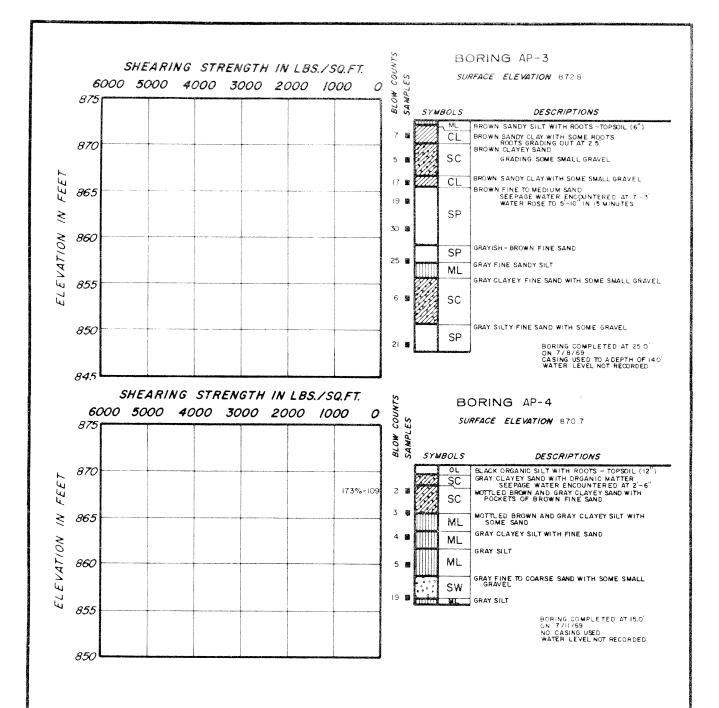
ATTACHMENT 1SITE LOCATION MAP



ATTACHMENT 2 BORING LOGS AND MONITORING WELL LOGS

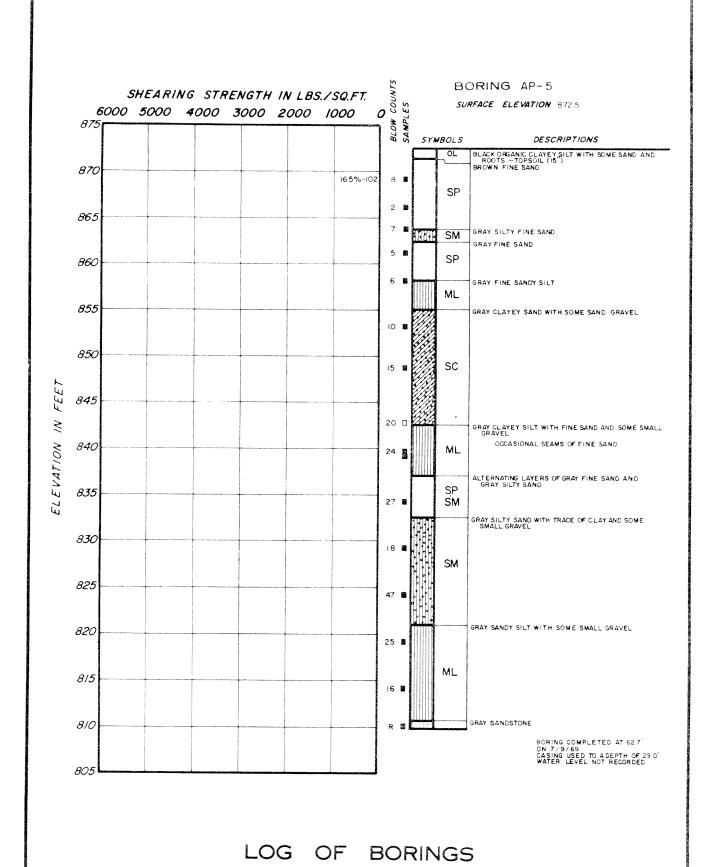


LOG OF TEST PITS

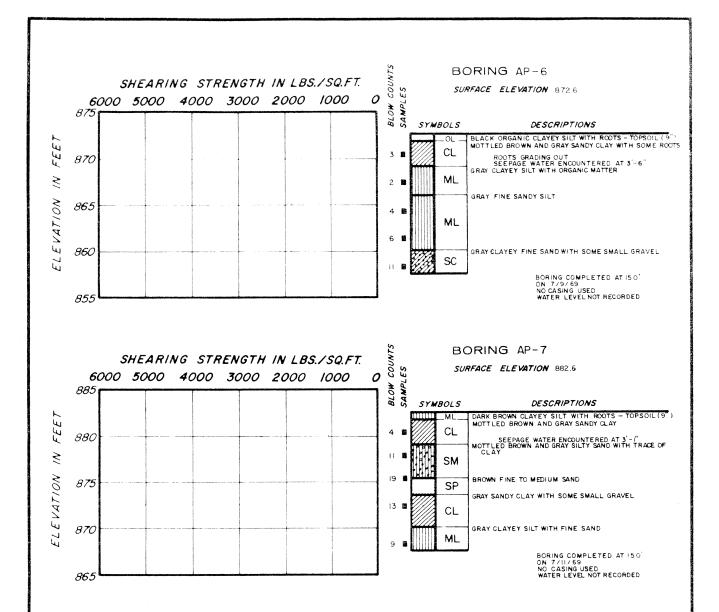


LOG OF BORINGS

CHECKED BY



DAMES 8 MOORE



LOG OF BORINGS

DAMES & MOORE



PROJECT:	LBWL - Erickson	PAGE	1 OF 1
PROJECT NO.:		BORING	CW-SB-01
ELEVATION:		DATE	10/2/2018
FIELD GEOLOG	GIST: Tim Mayotte	RIG	Geoprobe

	R		æ		MAT	ERIAL DESCRIPTION*			
SAMPLE NO., TYPE & DEPTH (ft)	BLOWS/SIX INCHES OR RQD (%)	SAMPLE RECOVERY/SAMPLE LENGTH (ft)	MATERIAL MOISTURE & WATER DEPTH (ft)	SOIL DENSITY/CONSISTENCY OR ROCK HARDNESS	COLOR	MATERIAL CLASSIFICATIO	Ν	USCS OR ROCK BROKENNESS	REMARKS
1						Void			
2									
3	NA	2.5 ft	Dry	Stiff	Gray-Brown	Sandy Clay		CL	
4			-						
5									
6									
7	NA	4 ft	Wet	Loose	Grav-Brown	Fine to Medium Sand		SP	Boring consists
8					,		7		of layers of
9									saturated soils
10		4 ft	Dry	Loose		Medium Sand		SP	from a depth of
11			,				-		5 ft to EOB.
12							T		3 It to LOB.
13							-		
14		4 ft	Moist	Loose		Medium to Coarse Sand	-	SP	
15		411	WOIST	Loose		Medium to Coarse Sand	-	35	
16			Wet	Stiff		Sandy Clay	23737373	SC-CL	
17			wei	Still		End of boring = 16 feet.		30-0L	
18						End of borning – To feet.			
19 20									
21 22									
23									
24 25									
									+
26									1
27									
28									
29 30									
									+
31									1
32									-
33									
34									
35									
36									
37									
38									
39									
40									

REMARKS Boring backfilled with bentonite chips.



PROJECT:	LBWL - Erickson	PAGE	1 OF 1
PROJECT NO.:		BORING	CW-SB-02
ELEVATION:		DATE	10/2/2018
FIELD GEOLOG	GIST: Tim Mayotte	RIG	Geoprobe

	-4		,		MAT	ERIAL DESCRIPTION*			
SAMPLE NO., TYPE & DEPTH (ft)	BLOWS/SIX INCHES OR RQD (%)	SAMPLE RECOVERY/SAMPLE LENGTH (ft)	MATERIAL MOISTURE & WATER DEPTH (ft)	SOIL DENSITY/CONSISTENCY OR ROCK HARDNESS	COLOR	MATERIAL CLASSIFICATIO	N	USCS OR ROCK BROKENNESS	REMARKS
1						Void			
2									
	NIA	2 #	Dmi	Stiff	O D	Clay		CI	
3	NA	3 ft	Dry	Suii	Gray-Brown/	Clay		CL	
4					Black				
5							(2)(2)(2)(2)		
6							-		
7	NA	4 ft	Wet	Loose	Gray-Brown	Medium Sand	-	SP	Boring consists
8							_		of layers of
9									saturated soils
10		4 ft	Moist	Loose	Gray-Brown	Medium Sand		SP	from a depth of
11									5 ft to EOB.
12									
13			Wet						
14		4 ft		Loose	Grav-Brown	Medium Sand		SP	
15		- 110	Moist	20000	Oldy Blown	Modiam Cana	7‱	0.	
16			Wolot				-		
17						End of boring = 16 feet.	<u> Paradaga</u>		
						End of borning – To reet.			
18									
19									
20									
21									
22									
23									
24									
25									
26									
27									
28									
29									
30									
31									
32									
33									
34									
35									
36									
37									
38									
39									
40									

REMARKS	Boring backfilled with bentonite chips.



PROJECT:	LBWL - Erickson	PAGE	1 OF 1
PROJECT NO.:		BORING	CW-SB-03
ELEVATION:		DATE	10/2/2018
FIELD GEOLOGI	ST: Tim Mayotte	RIG	Geoprobe

	-4				MAT	ERIAL DESCRIPTION*			
SAMPLE NO., TYPE & DEPTH (ft)	BLOWS/SIX INCHES OR RQD (%)	SAMPLE RECOVERY/SAMPLE LENGTH (ft)	MATERIAL MOISTURE & WATER DEPTH (ft)	SOIL DENSITY/CONSISTENCY OR ROCK HARDNESS	COLOR	MATERIAL CLASSIFICATIO	USCS OR ROCK BROKENNESS	REMARKS	
1						Void			
2									
	NΙΔ	2.25 ft	Dmi	Stiff	0	Clay		CI	
3	NA	2.25 ft	Dry	Suii	Gray-Brown	Clay		CL	
4									
5		_					(8)(8)(8)(8)		
6		_	Moist -				-		
7	NA	3 ft	Wet	Loose	Gray-Brown	Medium Sand	-	SP	Boring consists
8									of layers of
9									saturated soils
10		4 ft	Wet	Loose	Gray-Brown	Medium Sand		SP	from a depth of
11									5 ft to EOB.
12									
13									
14		4 ft	Moist -	Loose	Grav-Brown	Medium Sand		SP	
15			Wet	20000	City Brown	Modiam Cana	™	0.	
16			,,,,,				-		
17						End of boring = 16 feet.			
						End of borning – To reet.			
18									
19									
20									
21									
22									
23									
24									
25									
26									
27									
28									
29									
30									
31									
32									
33									
34									
35									
36									
37					1				
38									
39									
40									

REMARKS	Boring backfilled with bentonite chips.

GEOTECHNICAL TESTING SUMMARY

LBWL - Erickson Station - Foundation Samples MD&E Project No.



SAMPLE	CLASSIFICATION	%Fines	LL%	PI%	w% _{field}	$\mathbf{w}\%_{opt}$	ρ _d (lbs/ft³)	K (cm/s)
EW-F-01	Clayey Sand	29.50	NA	NA	NA	9.20	124.24	NA
EW-F-02	Clayey Sand	14.10	NA	NA	NA	8.25	129.23	NA
EW-F-03	Clayey Sand	9.70	NA	NA	NA	12.00	121.11	NA
EW-F-04	Clayey Sand	9.80	NA	NA	NA	8.50	125.92	NA
EW-F-05	Clayey Sand	16.30	NA	NA	NA	8.30	126.86	NA
EW-F-06	Clayey Sand	12.20	NA	NA	NA	7.85	131.10	NA
EW-T-01	Clayey Sand	NA	NA	NA	NA	10.00	133.60	NA
EW-T-02	Clayey Sand	NA	NA	NA	NA	9.80	127.67	NA
EW-T-03	Clayey Sand	NA	NA	NA	NA	9.30	127.98	NA
West Floor	Clayey Sand	13.10	NA	NA	NA	9.00	128.61	NA
South Floor	Clayey Sand	17.60	NA	NA	NA	7.95	129.98	NA
Ranges/Avera	ages:							

NOTES:

BORING ECT-18-B01

PAGE 1 OF 2



PROJECT NAME: LBWL New Gas Combined Cycle Plant

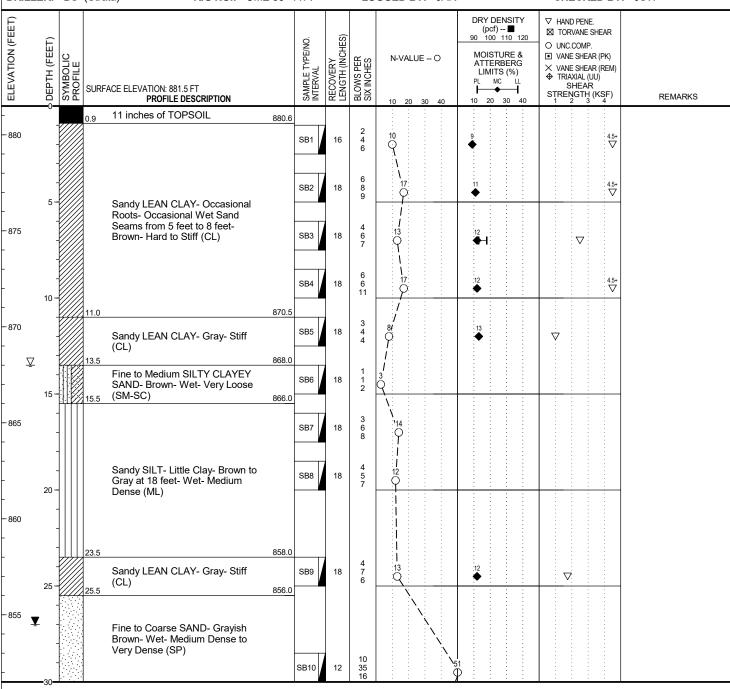
CLIENT: Lansing Board of Water & Light

PROJECT NUMBER: 079295.00

PROJECT LOCATION: Delta Township, Michigan

DATE STARTED: 6/28/18 **COMPLETED:** 6/28/18 **BORING METHOD:** Hollow-stem Augers

DRILLER: BS (Strata) RIG NO .: CME 55 - ATV LOGGED BY: JAR **CHECKED BY: JSW**



GROUNDWATER & BACKFILL INFORMATION

DEPTH (FT) ELEV (FT) 868.0

 ∇ DURING BORING: 13.5

▼ AT END OF BORING: 27.0 854.5

BACKFILL METHOD: Cement- Bentonite Grout

NOTES: 1. The indicated stratification lines are approximate. In situ, the transition between materials may be gradual.

2. Bulk sample obtained from auger cuttings while drilling from 0' to 10'





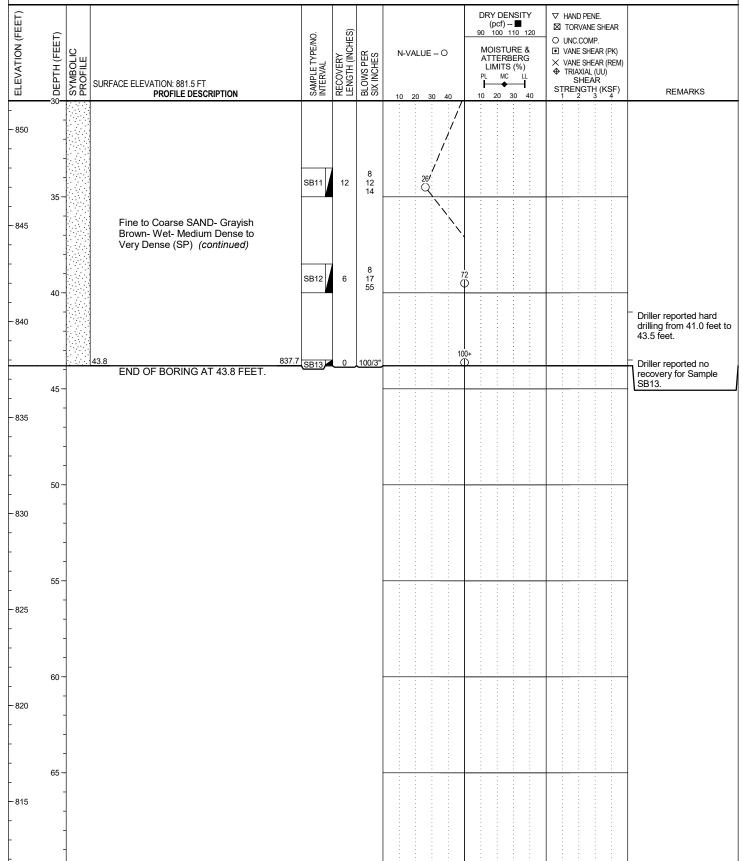


PROJECT NAME: LBWL New Gas Combined Cycle Plant

CLIENT: Lansing Board of Water & Light

PROJECT NUMBER: 079295.00

PROJECT LOCATION: Delta Township, Michigan



BORING ECT-18-B02

PAGE 1 OF 2



PROJECT NAME: LBWL New Gas Combined Cycle Plant

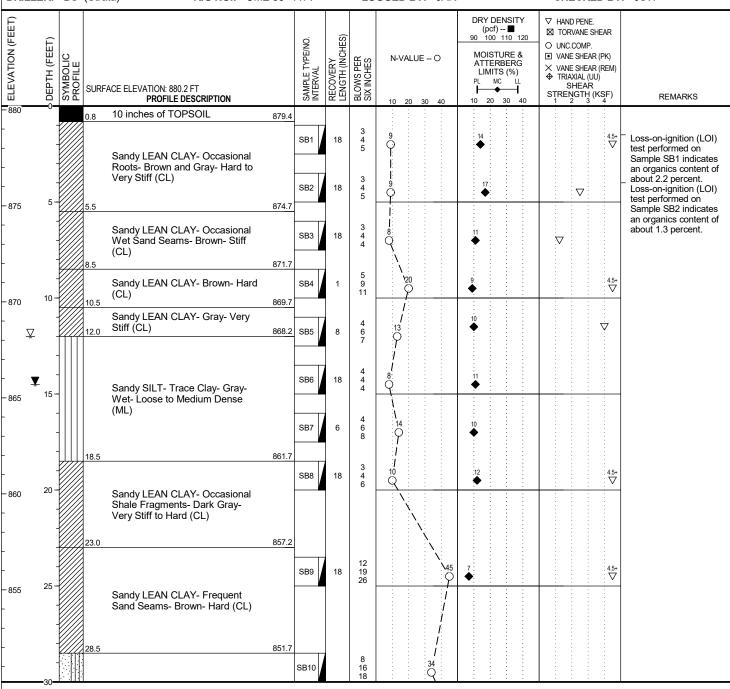
CLIENT: Lansing Board of Water & Light

PROJECT NUMBER: 079295.00

PROJECT LOCATION: Delta Township, Michigan

DATE STARTED: 6/29/18 COMPLETED: 6/29/18 BORING METHOD: Hollow-stem Augers

DRILLER: BS (Strata) RIG NO.: CME 55 - ATV LOGGED BY: JAR CHECKED BY: JSW



GROUNDWATER & BACKFILL INFORMATION

DEPTH (FT) ELEV (FT)

 ▼ DURING BORING:
 12.0
 868.2

 ▼ AT END OF BORING:
 14.5
 865.7

BACKFILL METHOD: Cement- Bentonite Grout

NOTES: 1. The indicated stratification lines are approximate. In situ, the transition between materials may be gradual.



PROJECT NAME: LBWL New Gas Combined Cycle Plant **PROJECT NUMBER:** 079295.00

CLIENT: Lansing Board of Water & Light		PROJECT LOCATIO	ROJECT LOCATION: Delta Township, Michigan				
SDEPTH (FEET) SYMBOLIC SYMBOLIC PROFILE SOLUTION: 880.2 LL BROGILE DESCRIPTION	SAMPLE TYPE/NO. INTERVAL RECOVERY LENGTH (INCHES) BI OWS PFR	N-VALUE O 11	DRY DENSITY (pcf) - ■ 90 100 110 120 MOISTURE & ATTERBERG LIMITS (%) PL MC LL ■ 0 20 30 40	▼ HAND PENE. ▼ TORVANE SHEAR ○ UNC.COMP. ■ VANE SHEAR (PK) × VANE SHEAR (REM) ◆ TRIAXIAL (UU) SHEAR STRENGTH (KSF) 1 2 3 4	REMARKS		
Fine to Coarse SAND with Silt and Gravel- Limestone pieces at 33.5 feet- Brown and Gray- Wet- Medium Dense (SP-SM) (continued) 846.6		0/1")+				
END OF BORING AT 33.6 FEET.	SB11						
-840 40 -							
-835 45 - 							
- 825 55							
-815 65-							
- - - - -							

BORING ECT-18-B03

PAGE 1 OF 2



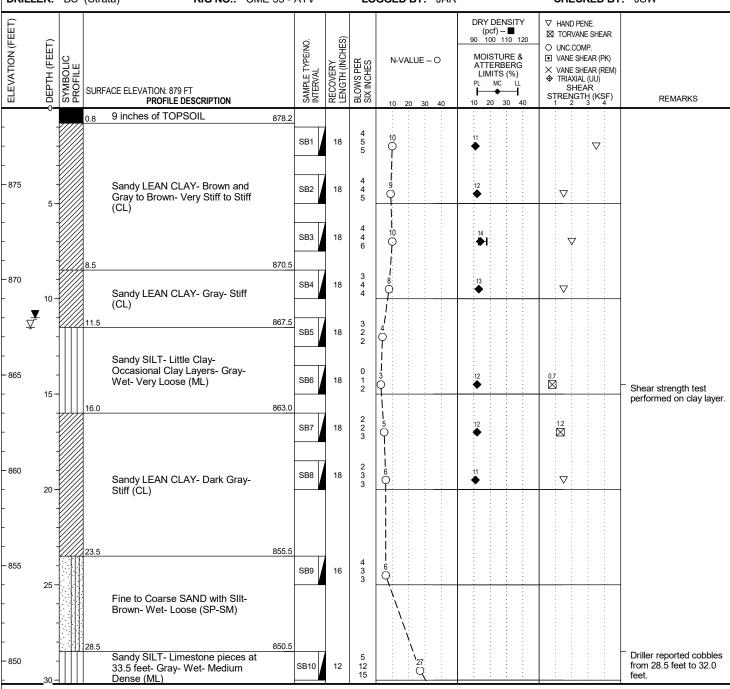
PROJECT NAME: LBWL New Gas Combined Cycle Plant

CLIENT: Lansing Board of Water & Light PROJECT LOCATION: Delta Township, Michigan

DATE STARTED: 6/28/18 COMPLETED: 6/28/18 BORING METHOD: Hollow-stem Augers

DRILLER: BS (Strata) RIG NO.: CME 55 - ATV LOGGED BY: JAR CHECKED BY: JSW

PROJECT NUMBER: 079295.00



GROUNDWATER	& BACKFILL INFORMATION	

DEPTH (FT) ELEV (FT) 11.5 867.5

 ▼ DURING BORING:
 11.5
 867.5

 ▼ AT END OF BORING:
 11.0
 868.0

BACKFILL METHOD: Cement- Bentonite Grout

NOTES: 1. The indicated stratification lines are approximate. In situ, the transition between materials may be gradual.

2. Bulk sample obtained from auger cuttings while drilling from 0' to 10'

(Continued Next Page)



BORING ECT-18-B03

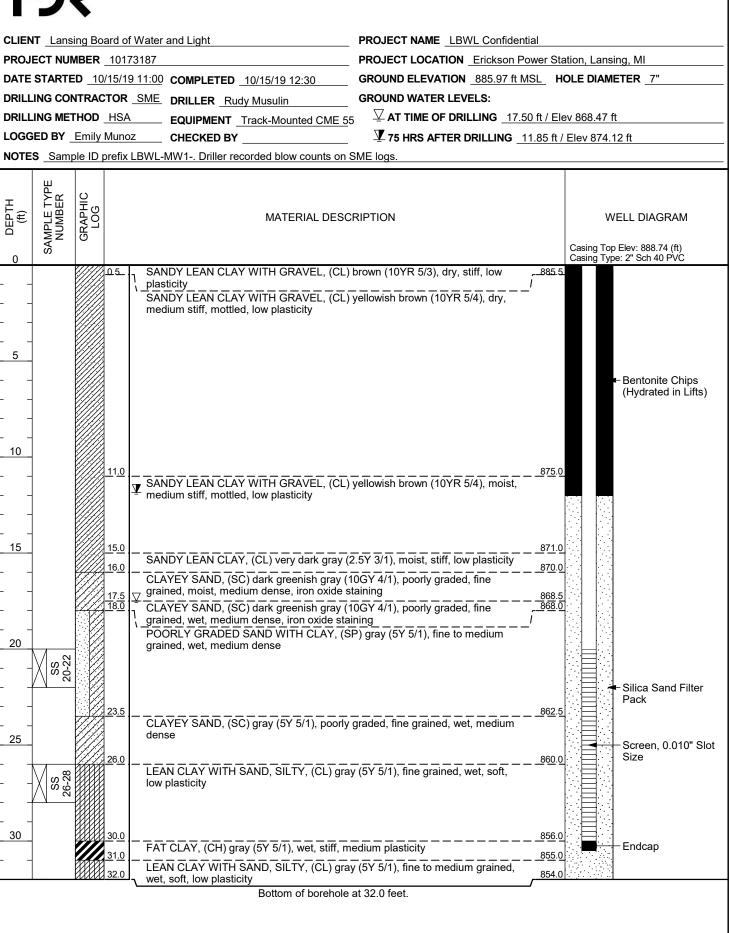
PAGE 2 OF 2

PROJECT NAME: LBWL New Gas Combined Cycle Plant PROJECT NUMBER: 079295.00

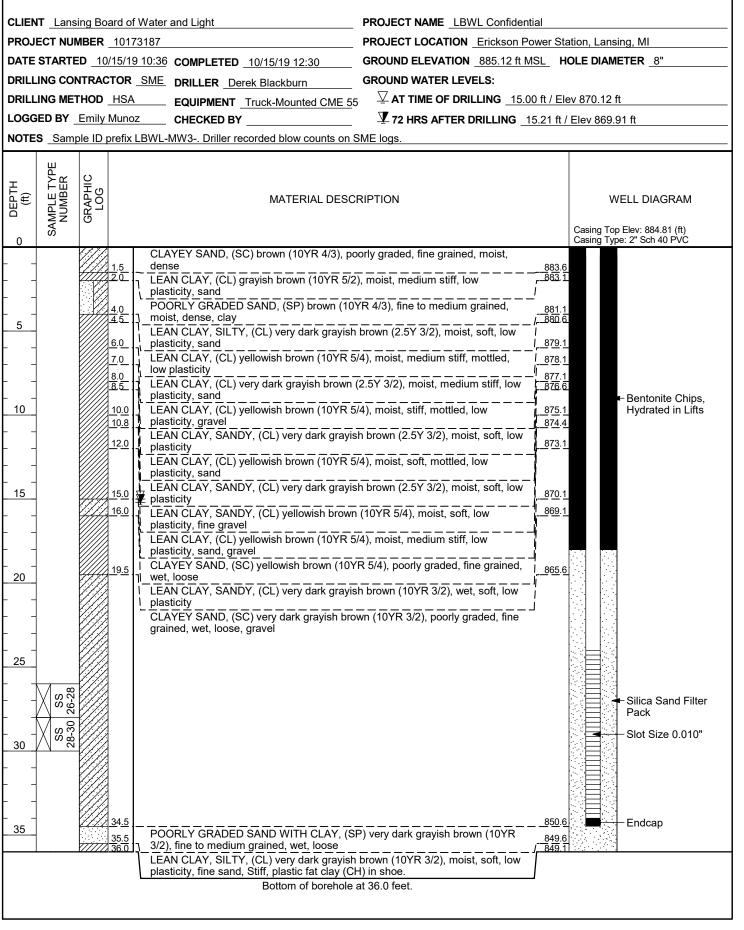
PPO IFCT I OCATION: Delta Township Michig

Company Comp	CLIEN	CLIENT: Lansing Board of Water & Light			PROJECT LOCATION: Delta Township, Michigan							
833 Feet. SEND OF BORING AT 33.7 FEET.	ELEVATION (FEET)	DEPTH (FEET)	SYMBOLIC PROFILE	SURFACE ELEVATION: 879 FT PROFILE DESCRIPTION		RECOVERY LENGTH (INCHES)	BLOWS PER SIX INCHES		(pcf) ■ 90 100 110 120 MOISTURE & ATTERBERG LIMITS (%) PL MC IL — ← — I	☑ TORVANE SHEAR○ UNC.COMP.☑ VANE SHEAR (PK)	REMARKS	
- 845	-	- - -		33 7 845.3	SR11	1 .	50/2"	50+			Driller reported hard dilling from 32.0 feet to 33.7 feet.	
-840	-845	25		END OF BORING AT 33.7 FEET.	0011)							
- 40		-										
- 40	-	-										
- 40	-	-										
-835 - 45 50	-840	-										
- 45		40 -										
- 45	-	-										
- 45	-	-										
- 830 50	- 835	-										
- 825		45 -										
- 825	_	-										
- 825	-	-										
- 825	-830	-										
- 55- 	-	50 -										
- 55- 		_										
- 55- 	_	-										
- 820 60	-825	-										
- 60	-	55 –										
- 60												
- 60	_	_										
	-820	-										
- 65 - - 810 -	_	60 –										
- 65 - - 810 -	-	-										
- 65 - - 810 -		-										
 -810 -	-815	-										
	-	65 –										
	-	-										
	-	-										
	- 810	-										
	-	70 –										



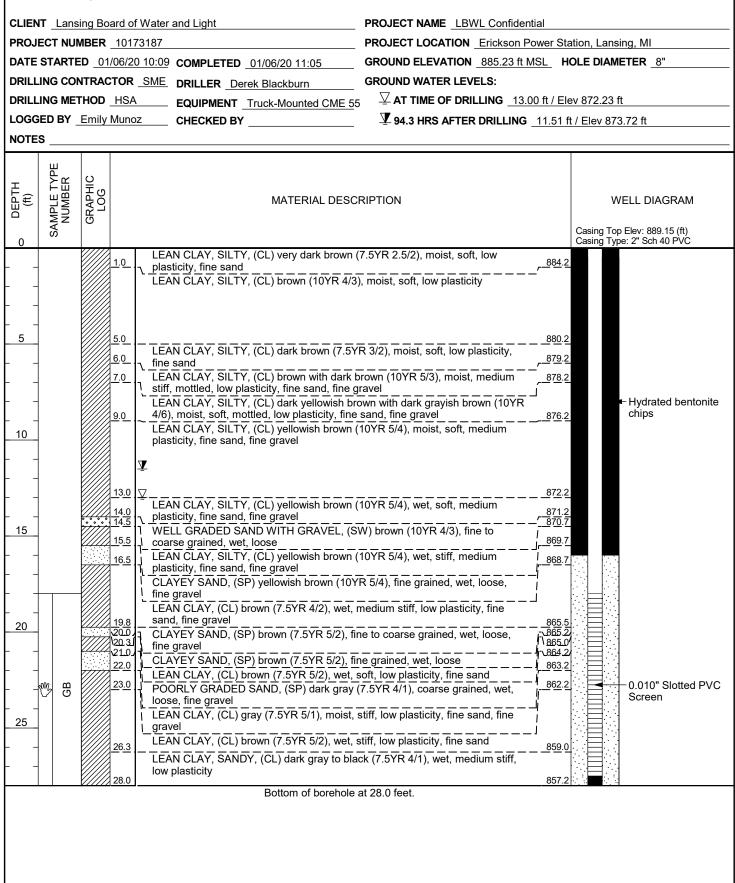




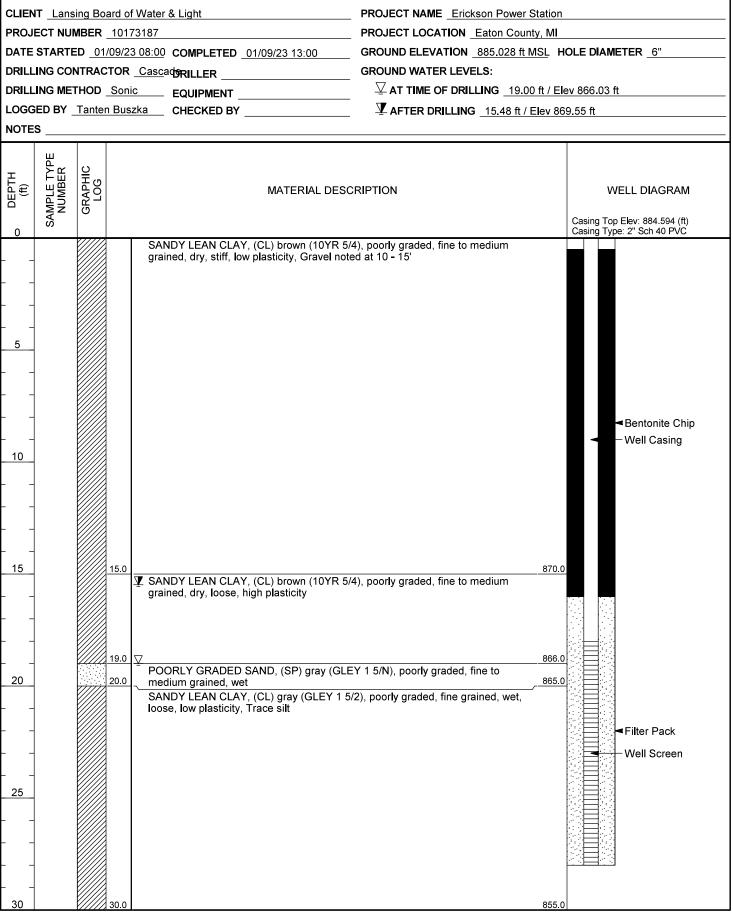




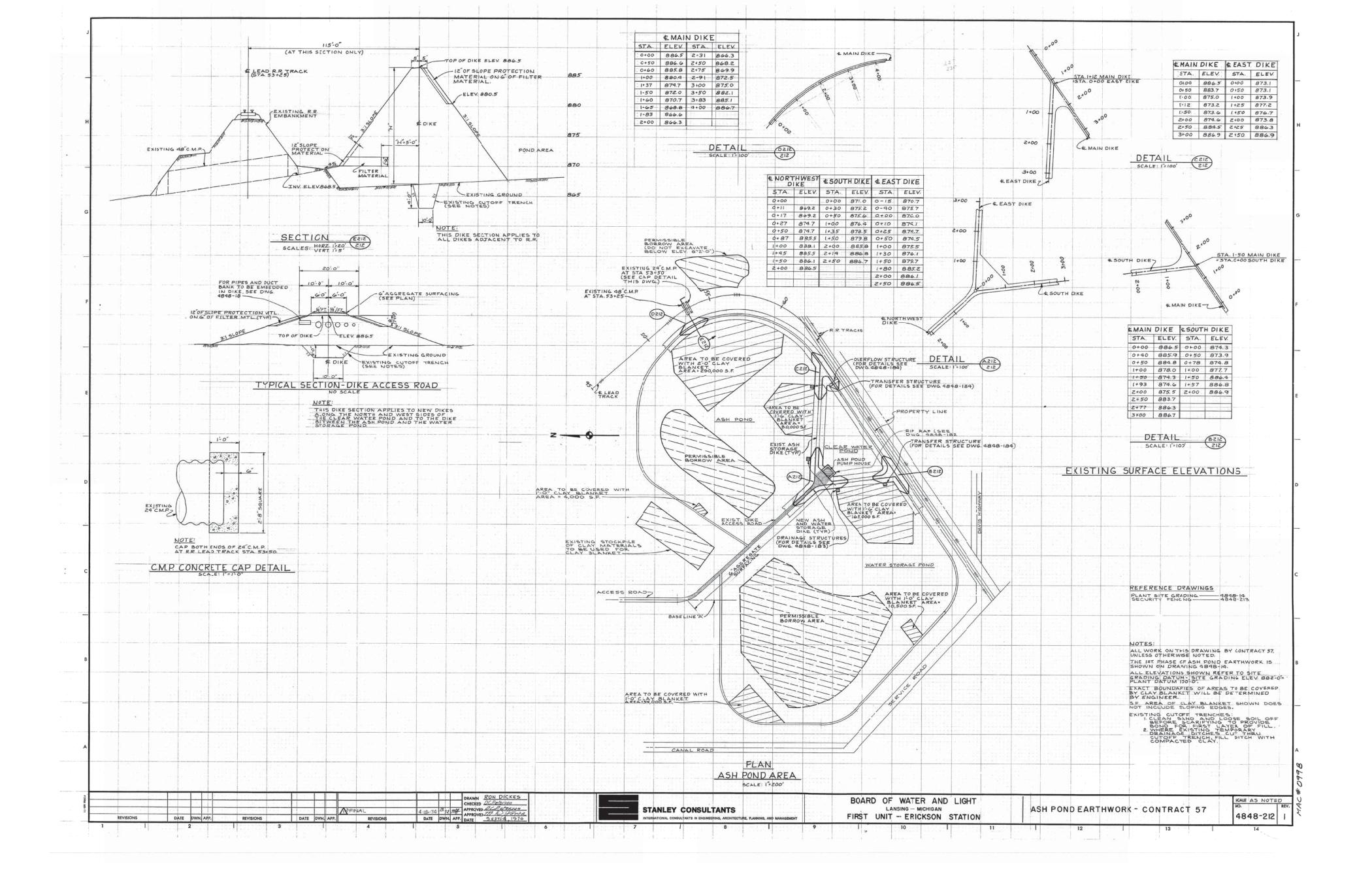


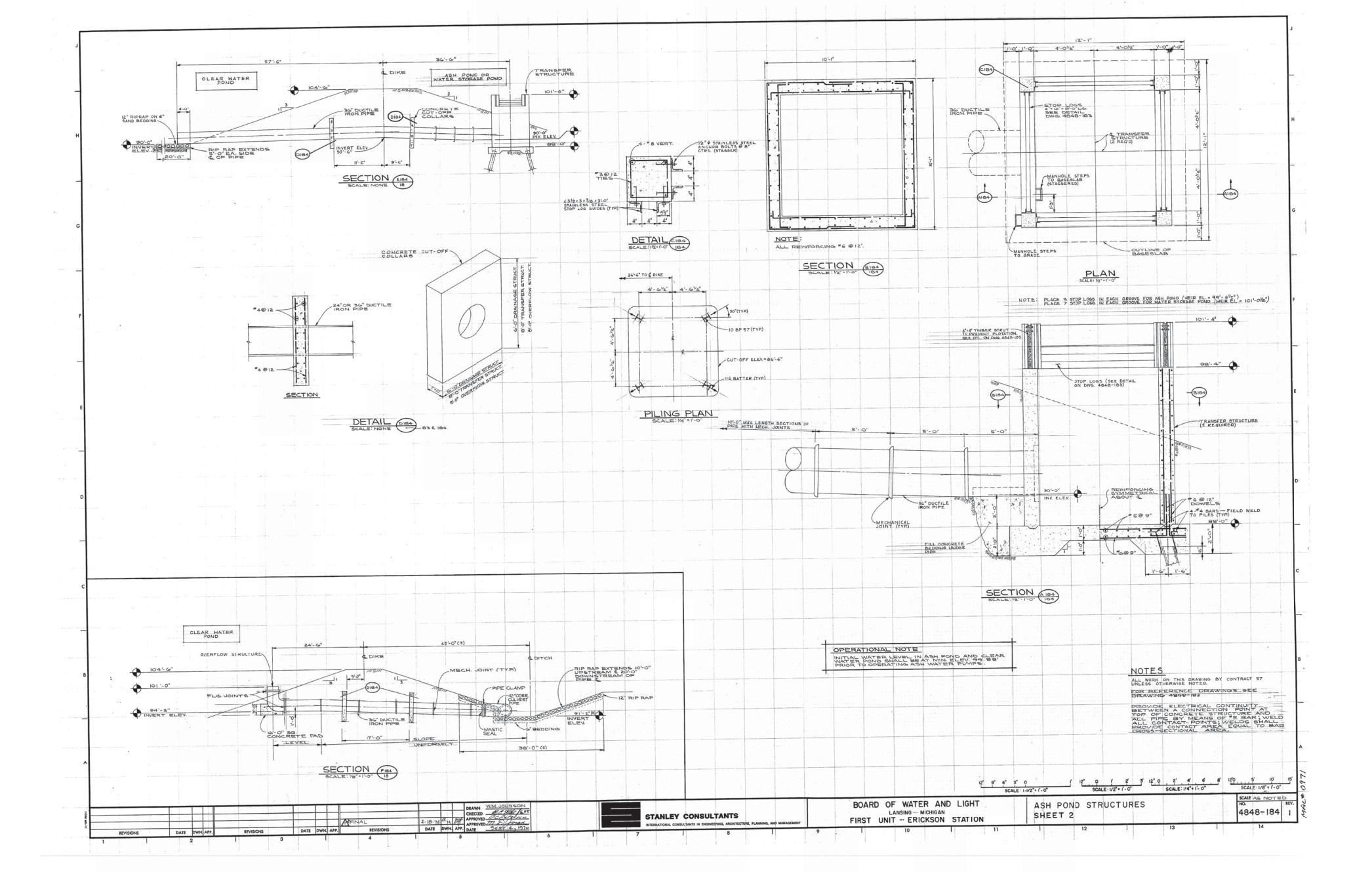




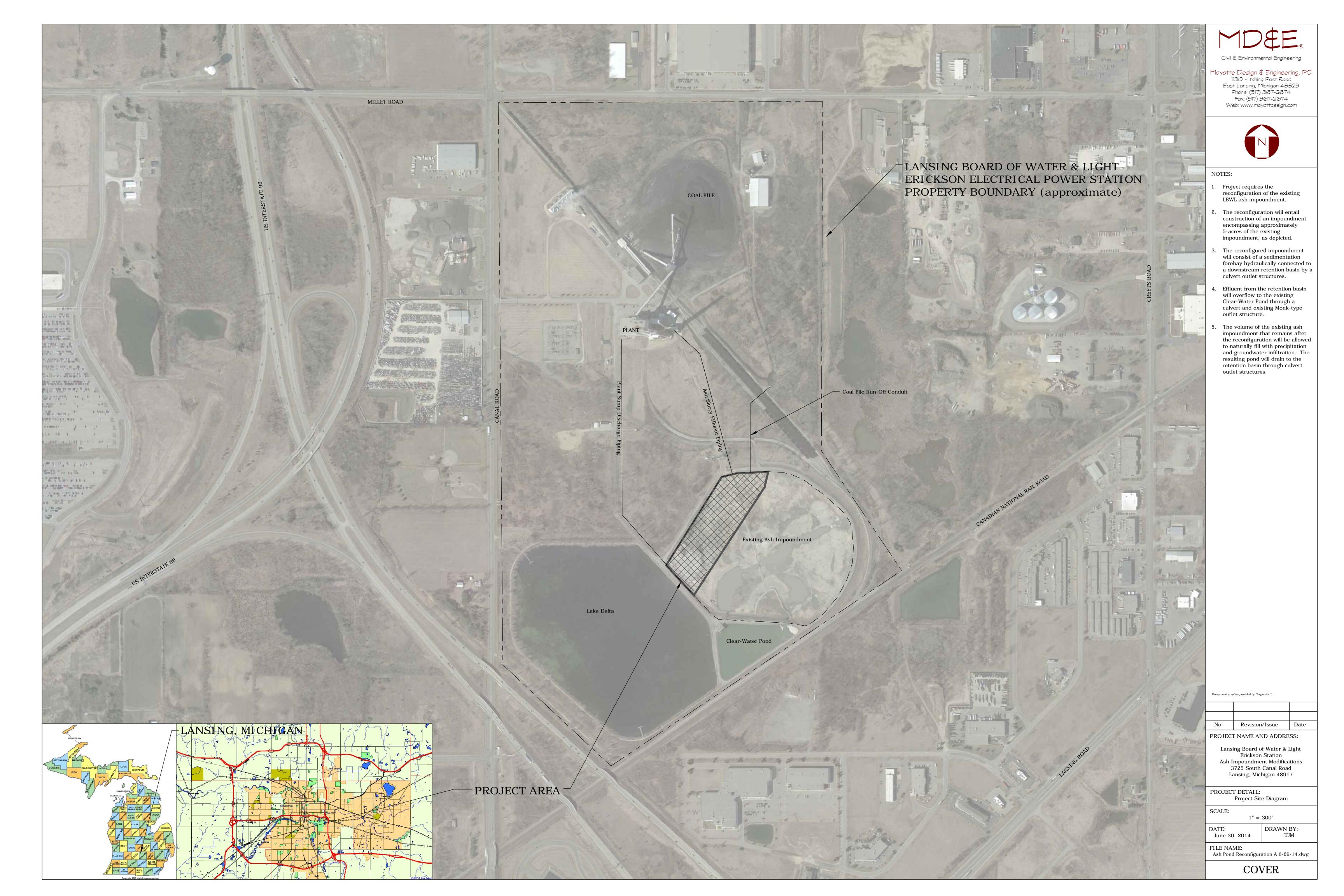


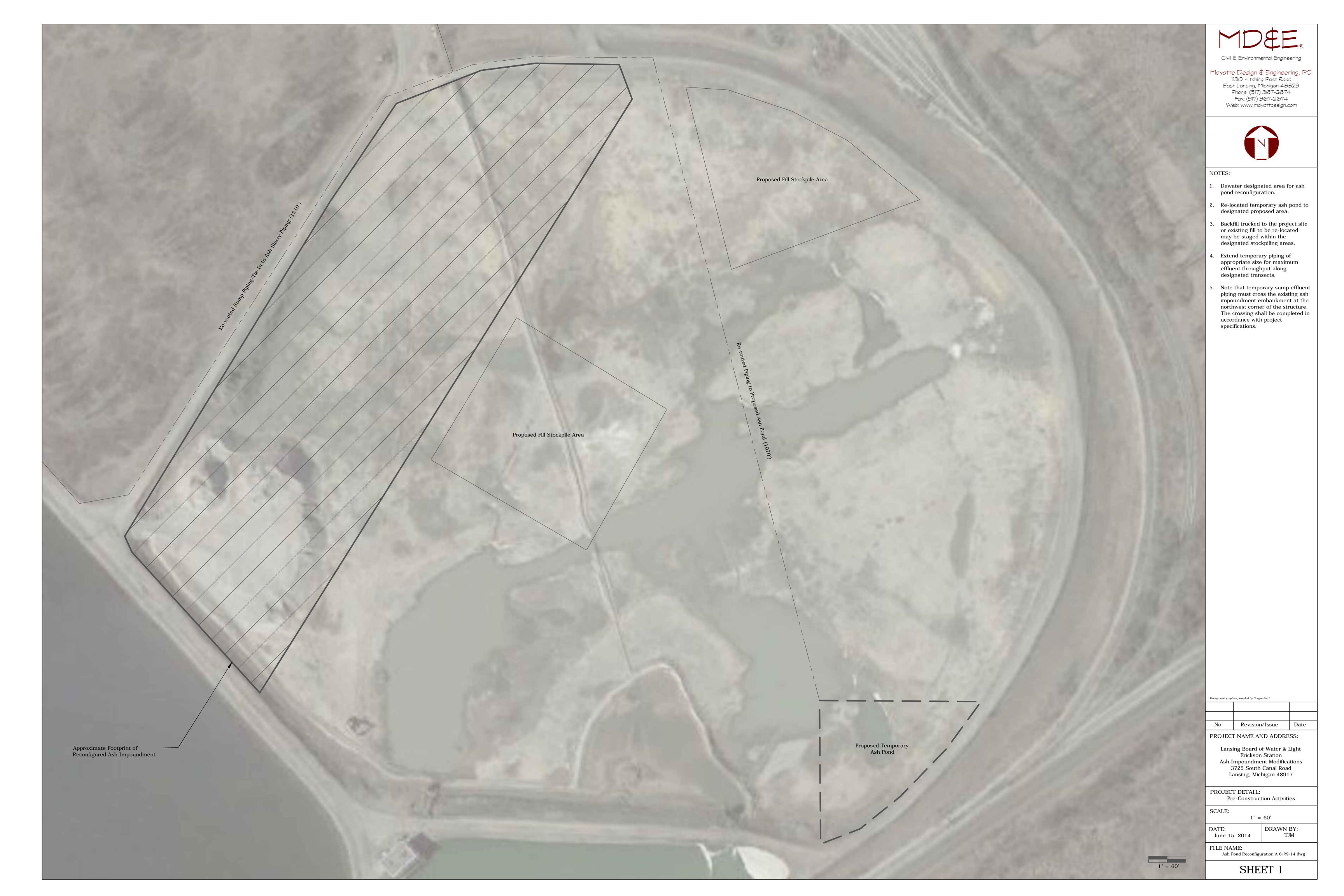
ATTACHMENT 31970 CONSTRUCTION DRAWINGS

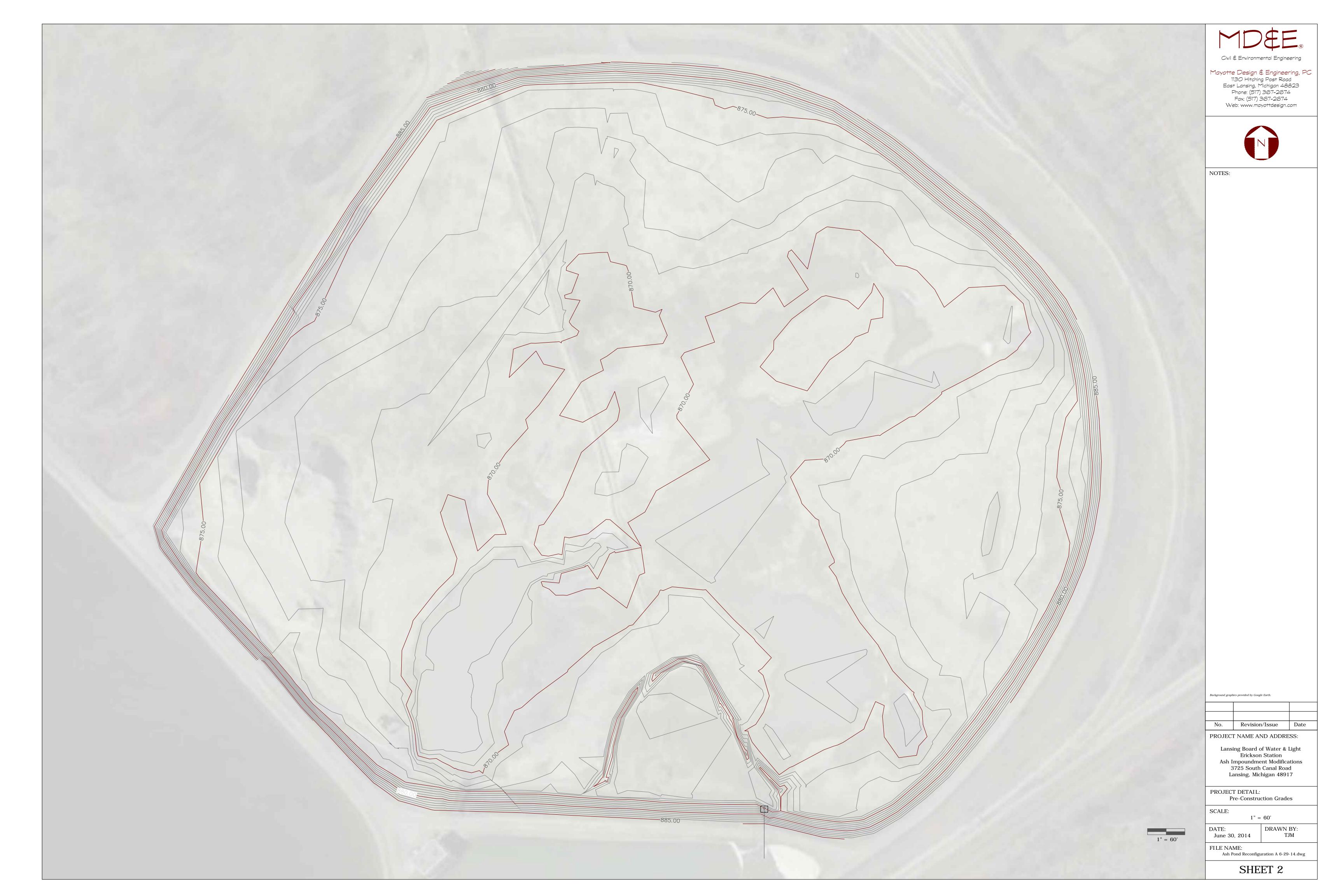




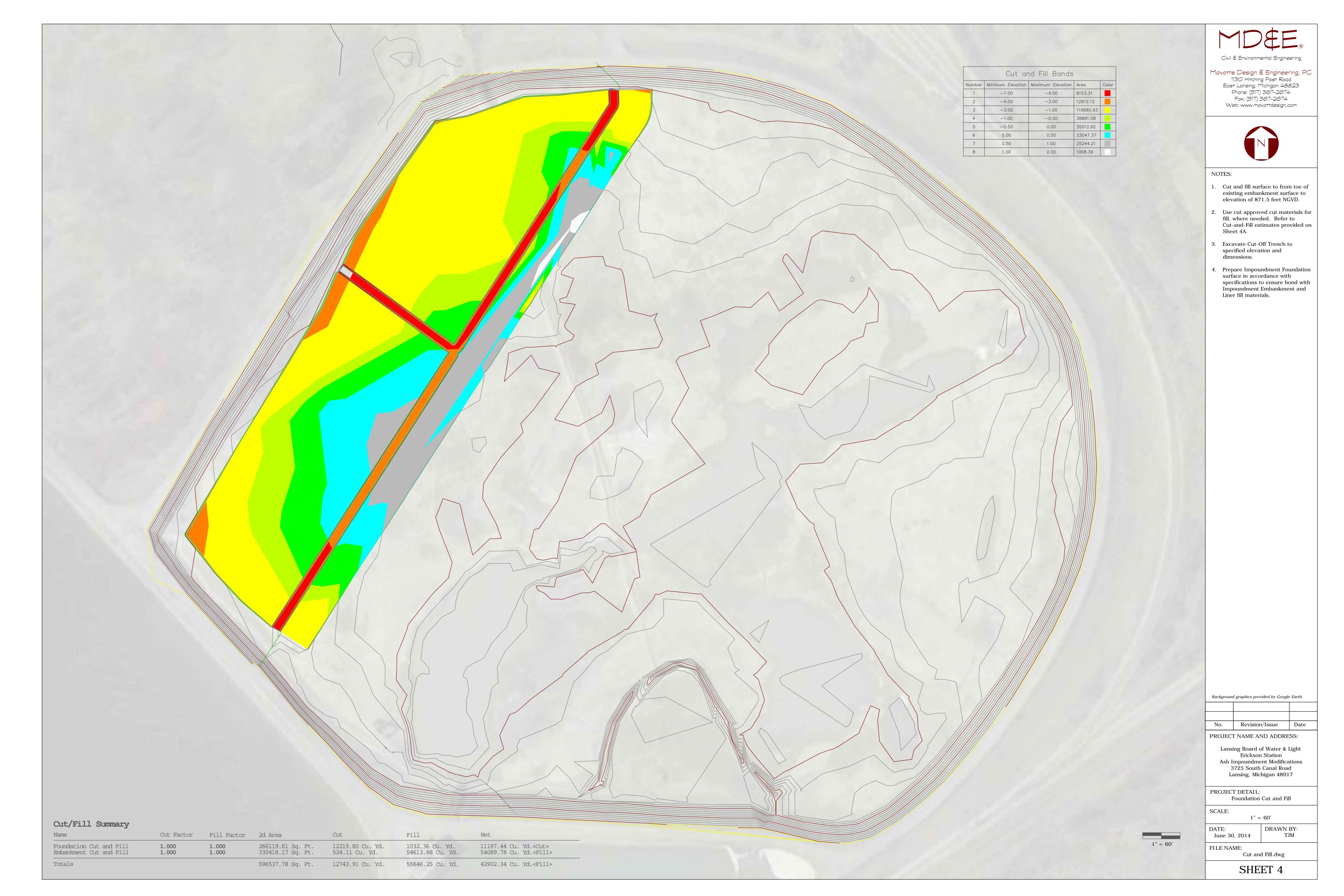
ATTACHMENT 4 CONSTRUCTION DRAWINGS FOR FORMER FOREBAY AND FORMER RETENTION BASIN

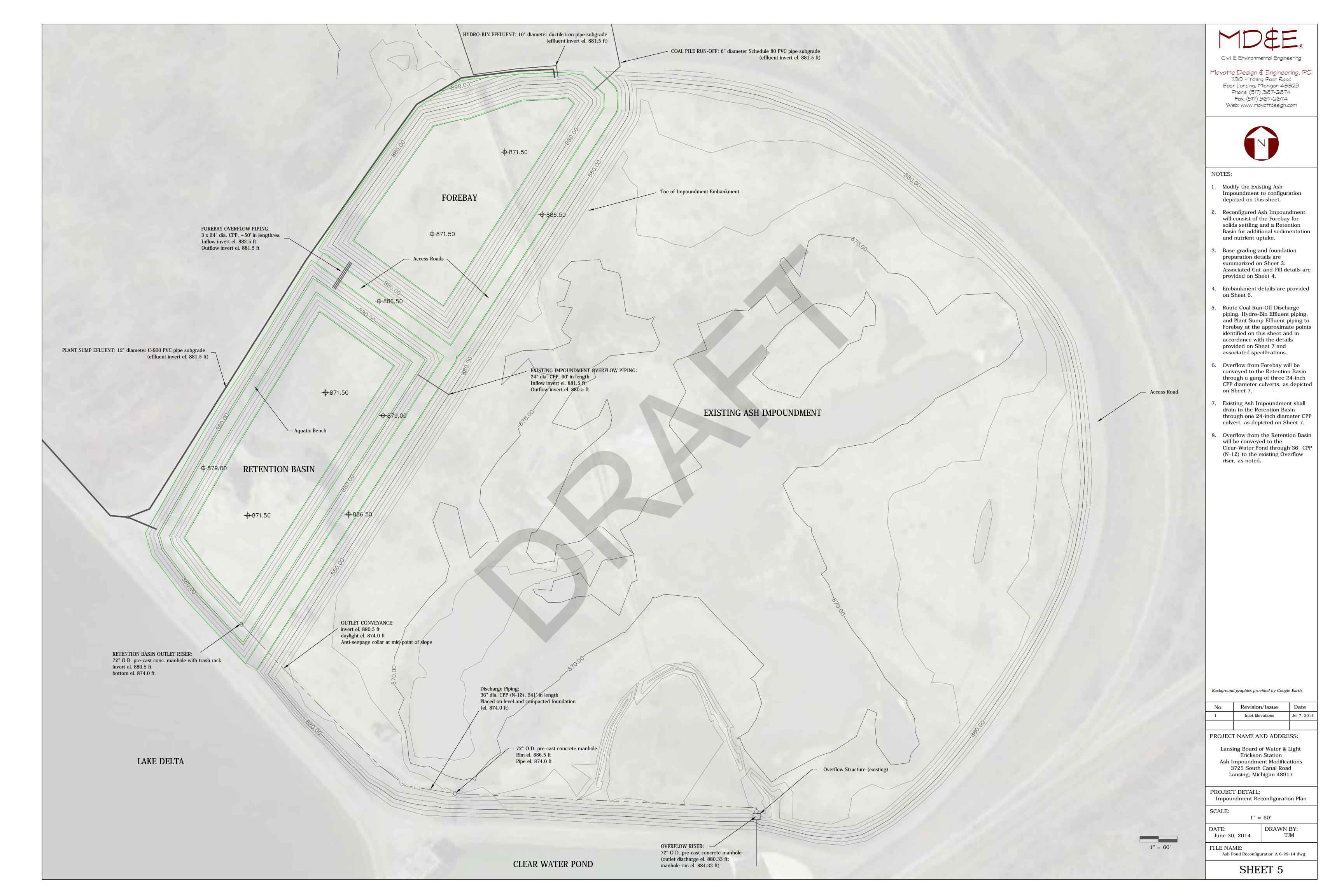


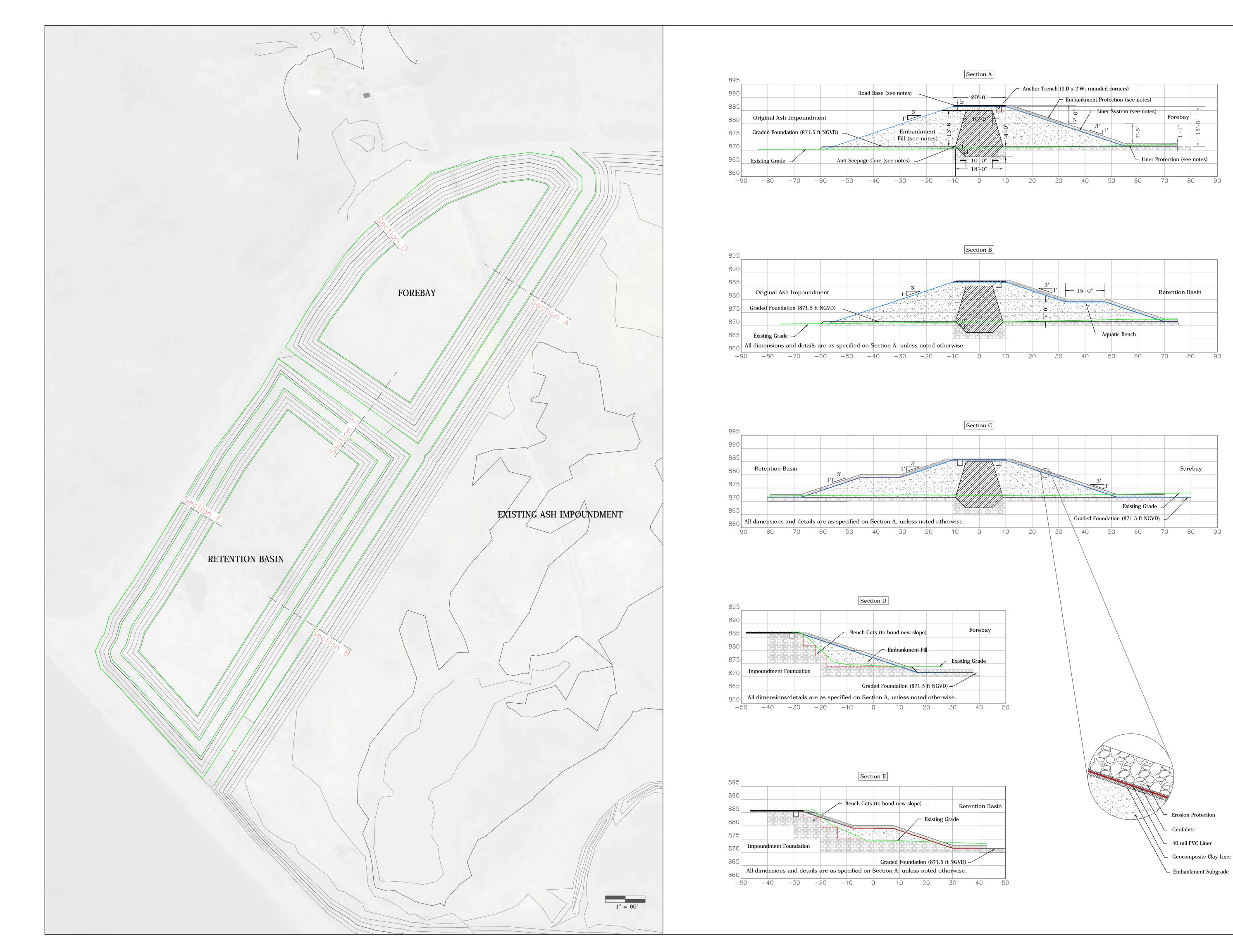














Civil & Environmental Engineering

Mayotte Design & Engineering, PC 1130 Hitching Post Road
East Lansing, Michigan 48823
Phone: (517) 367-2674
Fax: (517) 367-2674 Web: www.mayottdesign.com



- 1. All dimensions are in feet and
- 2. Embankment Fill material: should conform to Unified Soil
- 3. Anti-Seepage Core material: should conform to Unified Soil Classification GC, SC, CL or CH and maintain a permeability of less than 10E-7 cm/s following

compaction.

Classification SP or SC.

- 4. Synthetic Liner System: 40 mil PVC liner over Geocomposite clay liner (Bentomat ST).
- Existing embankments shall be benched per specifications to create a bond with new embankment fill.
- 6. Embankment protection materials shall be 2" x 5" crushed concrete over a suitable geotextile mat.
- 7. Liner protection materials shall consist of fine-grained granular aggregate over a suitable geotextile mat.
- 8. Road Base materials: should be 22-1A crushed concrete placed to a depth of 4-6".
- 9. See specifications for placement, compaction and testing requirements for the materials specified above.

Forebay

Revision/Issue Date

PROJECT NAME AND ADDRESS:

Lansing Board of Water & Light Erickson Station Ash Impoundment Modifications 3725 South Canal Road Lansing, Michigan 48917

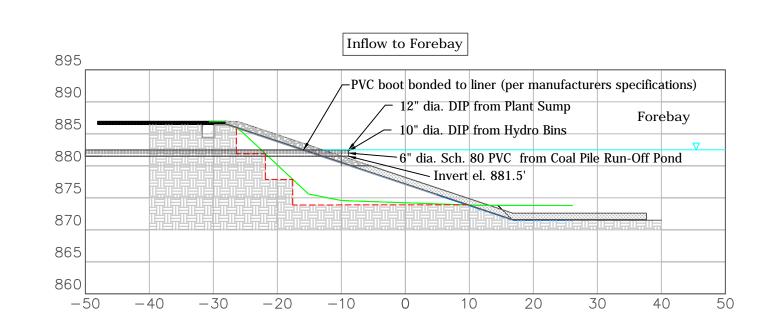
PROJECT DETAIL: Typical Embankment Details

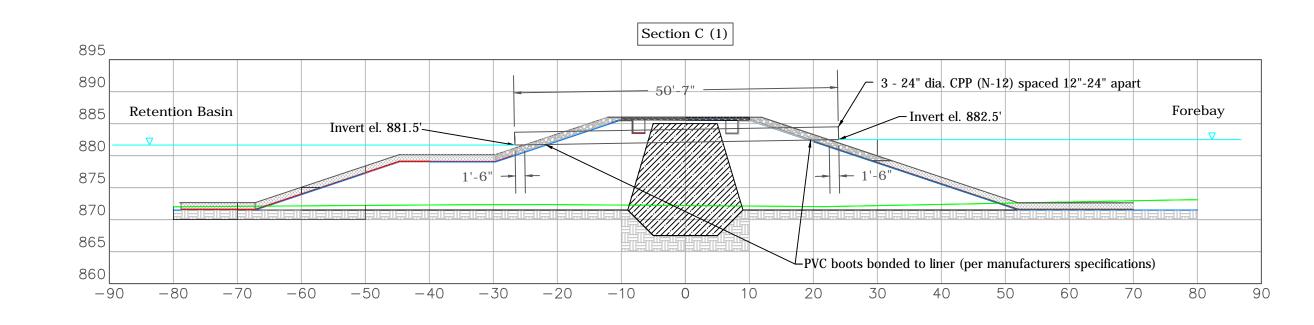
SCALE:

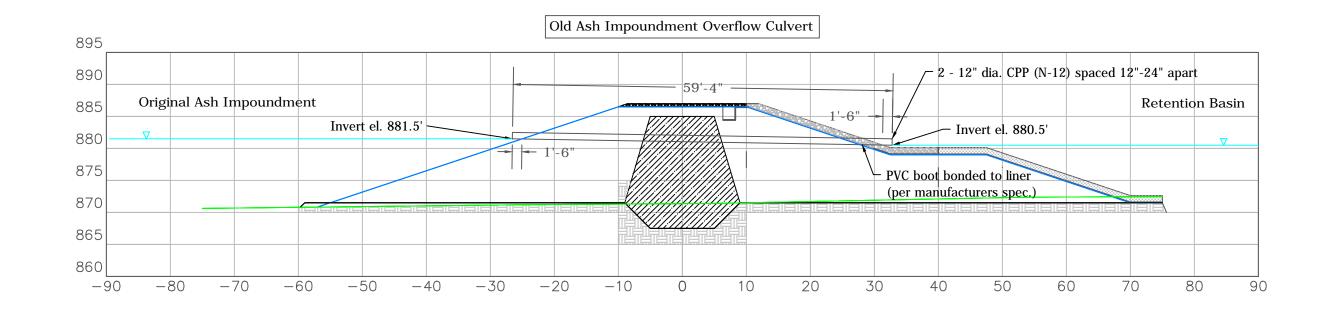
1'' = 60'DRAWN BY: June 30, 2014

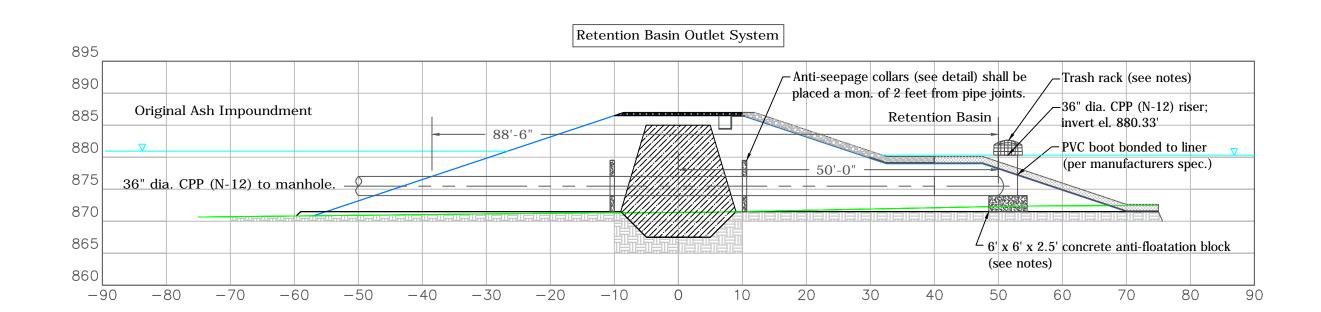
FILE NAME: Ash Pond Reconfiguration A Profiles.dwg

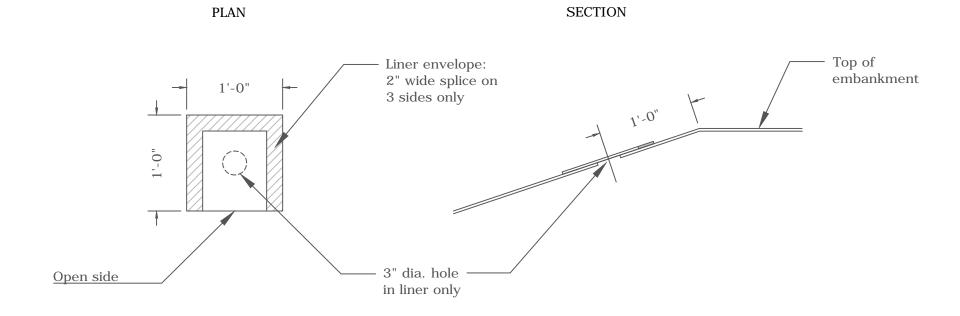
SHEET 6



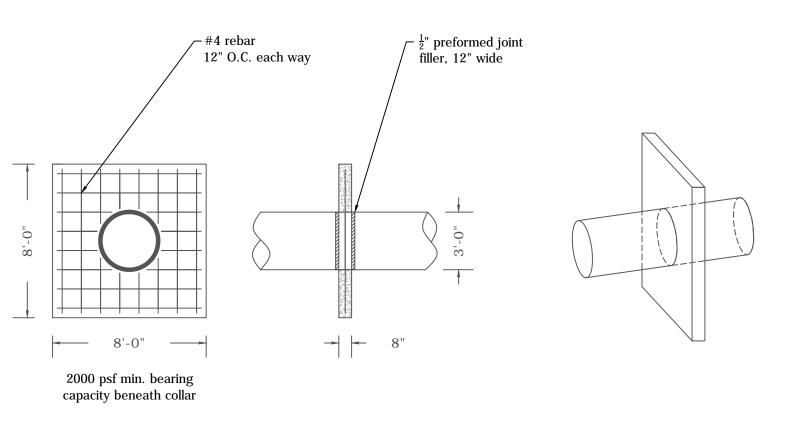




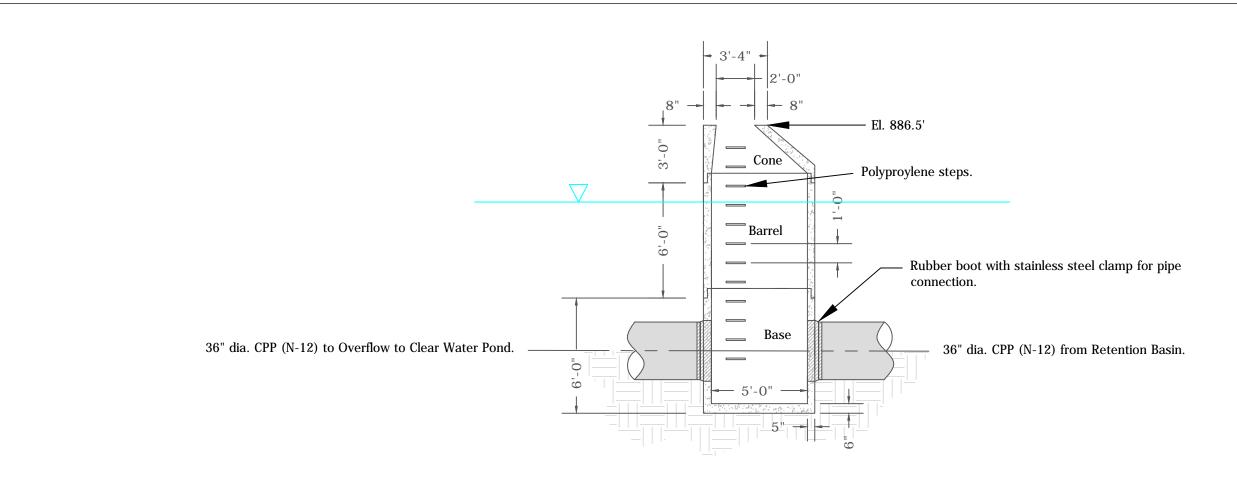




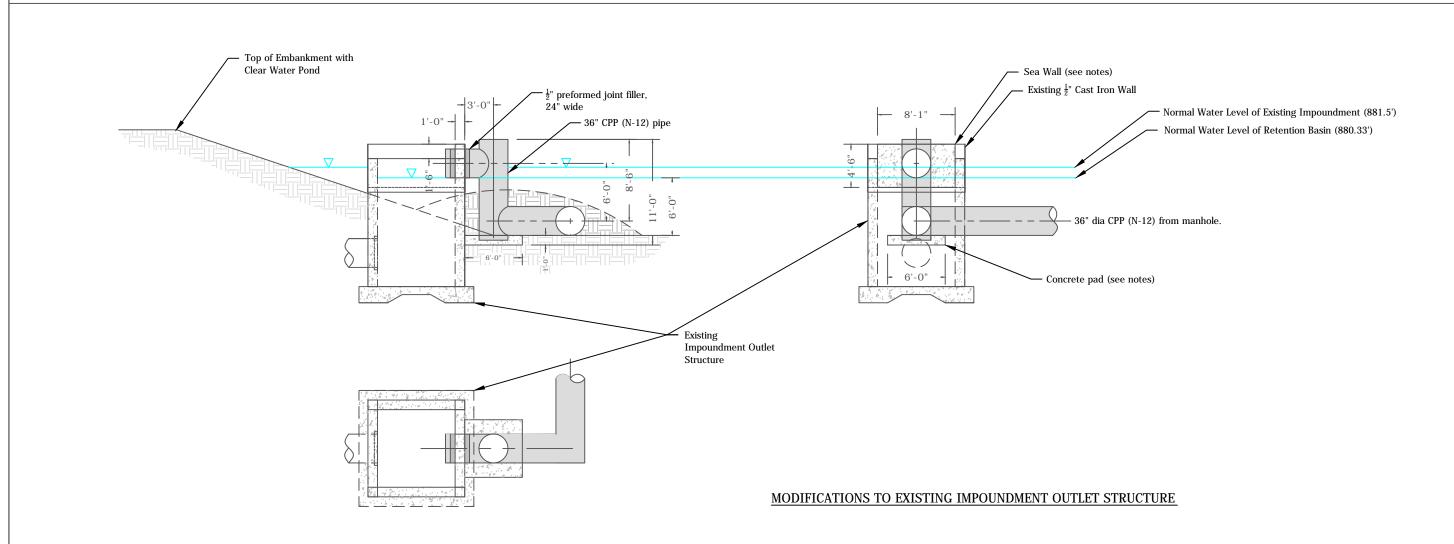
AIR/GAS VENT DETAIL



ANTI-SEEPAGE COLLAR



PRE-CAST MANHOLE





Civil & Environmental Engineering

Mayotte Design & Engineering, PC 1130 Hitching Post Road East Lansing, Michigan 48823 Phone: (517) 367-2674 Fax: (517) 367-2674 Web: www.mayottdesign.com



NOTES:

- 1. All poured concrete shall be min. 3,000 psi (28 day), unless noted otherwise.
- 2. Concrete anti-floatation block shall be integrally attached to riser base to prevent riser/block separation.
- 3. Trash Rack: Contech Construction Products Inc. Round Series, RS-48.
- 4. Air/Gas Vents to be positioned as detailed on 30' centers around both the Forebay and Retention
- 5. Pre-cast manhole to be constructed of 4000 psi concrete
- (at 28 days).6. Manhole to be designed for H-20

wheel loading.

- 7. Manhole construciton to conform to ASTM C-478 and MDOT specifications.
- 8. Manhole concrete to be reinformced to 0.12 in sq/L.F.
- 9. Mahole shiplap joints to be sealed with butyl rubber gaskets.
- 10. Concrete block for overflow structure shall be integrally attached to riser base to prevent riser/block separation.
- 11. Sea Wall shall be reinforced with #4 rebar, 12" O.C. each direction.

Background graphics provided by Google Earth.

No. Revision/Issue Date

Lansing Board of Water & Light Erickson Station Ash Impoundment Modifications 3725 South Canal Road Lansing, Michigan 48917

PROJECT NAME AND ADDRESS:

PROJECT DETAIL: As Noted

SCALE:

Varies

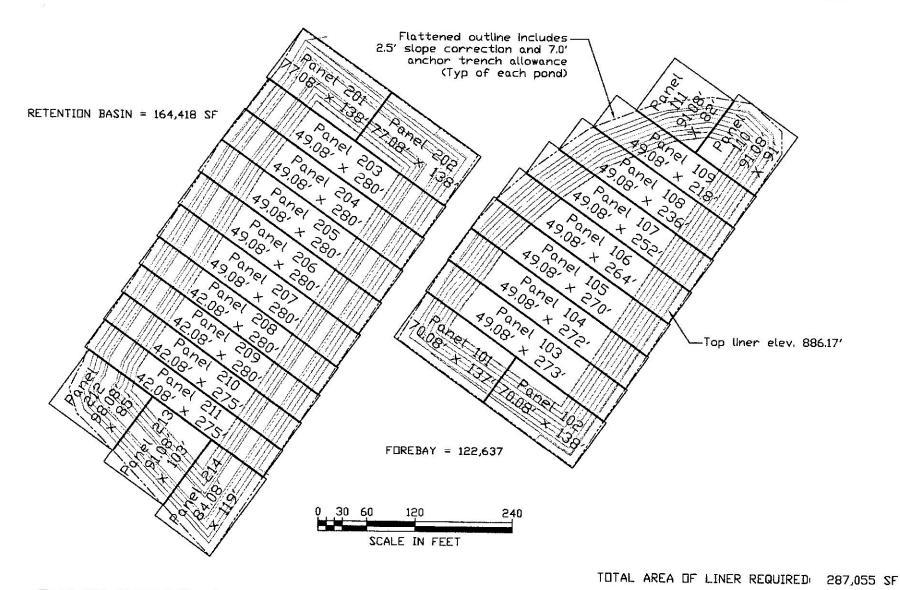
DRAWN BY:

June 30, 2014 TJM
FILE NAME:

Ash Pond Reconfiguration A Profiles.dwg

SHEET 7

	REVISIONS		
REV	DESCRIPTION	DATE	APPROVED







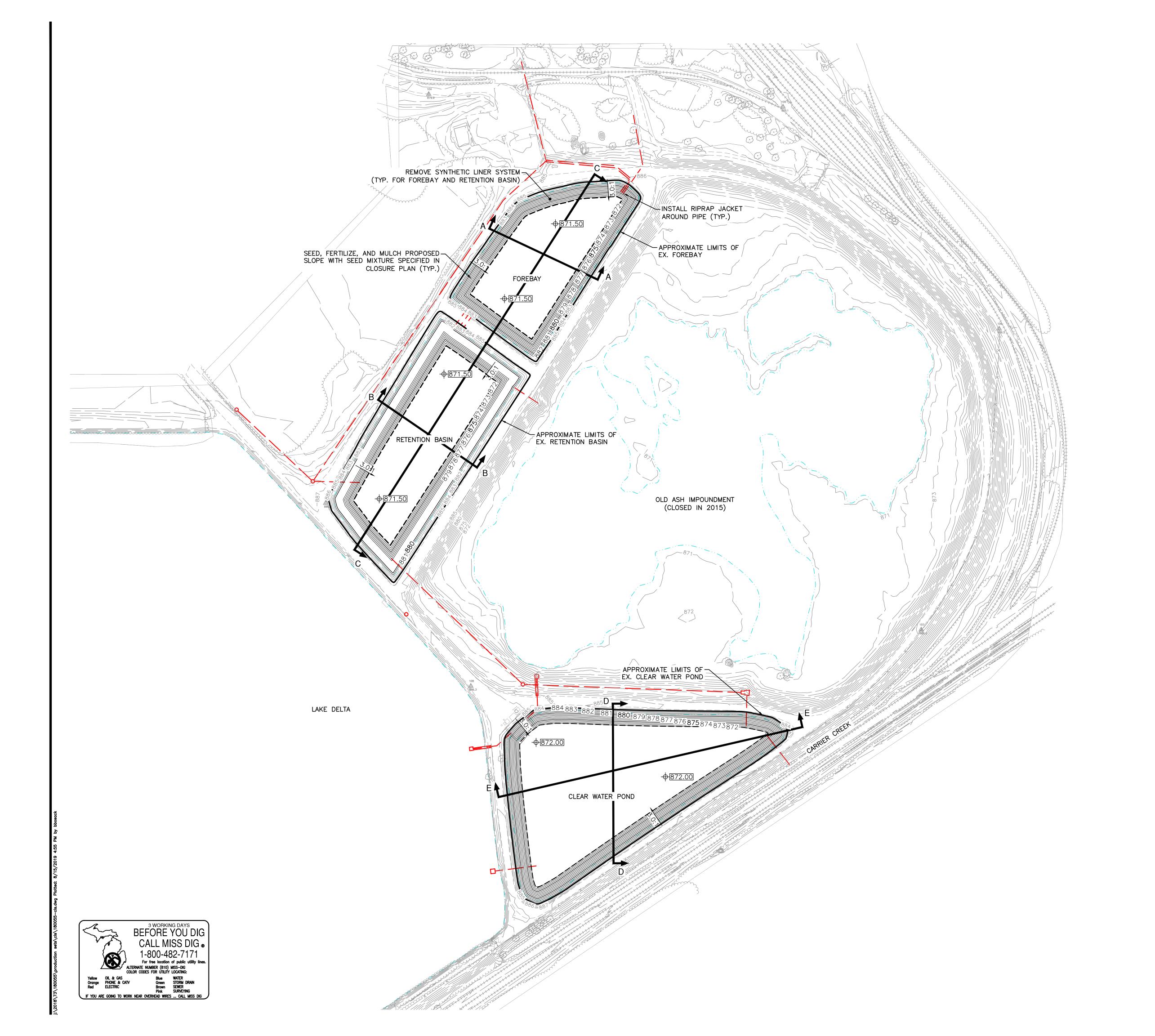
LANGE CONTAINMENT SYSTEMS, INC.

5150 RACE COURT DENVER, CO 80216 (303) 446-8644 FAX (303) 446-8798

Lansing Water & Light

40 Mil PVC Liner for Retention and Forebay Basins

ATTACHMENT 52018 GRADING PROFILES





LEGEND

EXISTING CONTOURS

EXISTING RAILROAD TRACK

EXISTING FENCE

EXISTING EDGE OF WATER

EXISTING CONVEYANCE PIPE

EXISTING DRIVEWAY

EXISTING VEGETATION

EXISTING TREE

PROPOSED CONTOURS

PROPOSED SPOT ELEVATION

1%—PROPOSED SLOPE

NOTES:

- EXISTING TOPOGRAPHIC SURVEY COMPLETED BY DRONEVIEW ON SEPTEMBER 26, 2018. VERTICAL DATUM IS IN NAVD 88.
- 2. NO POND BOTTOM SOUNDING WAS PERFORMED FOR THE FOREBAY AND RETENTION BASIN. ASH VOLUME ESTIMATED BASED ON REMOVAL EFFICIENCY OF PLANT HYDROBINS.
- 3. BOTTOM OF ASH LIMITS FOR FOREBAY AND RETENTION BASIN BASED ON INFORMATION PROVIDED IN THE CONSTRUCTION DOCUMENTATION REPORT FOR THE ASH IMPOUNDMENT RECONFIGURATION BY MAYOTTE DESIGN AND ENGINEERING, P.C., DATED MAY
- 4. BOTTOM OF ASH LIMITS FOR CLEAR WATER POND BASED ON HISTORICAL PLANT DRAWINGS 4848-183 "ASH POND STRUCTURES SHEET 1" AND 4848-184 "ASH POND STRUCTURES SHEET 2".



NTH Consultants, Ltd.
Infrastructure Engineering and

Northville, MI 248.553.6300
Detroit, MI 313.237.3900
Lansing, MI 517.484.6900
Grand Rapids, MI 616.451.6270
Cleveland, OH 216.334.4040

Environmental Services

SUBMITTAL						
REV	DESCRIPTION	DATE	BY			
PROJECT NAME:						

PROJECT LOCATION:

ERICKSON STATION LANSING, MICHIGAN

ERICKSON STATION ASH

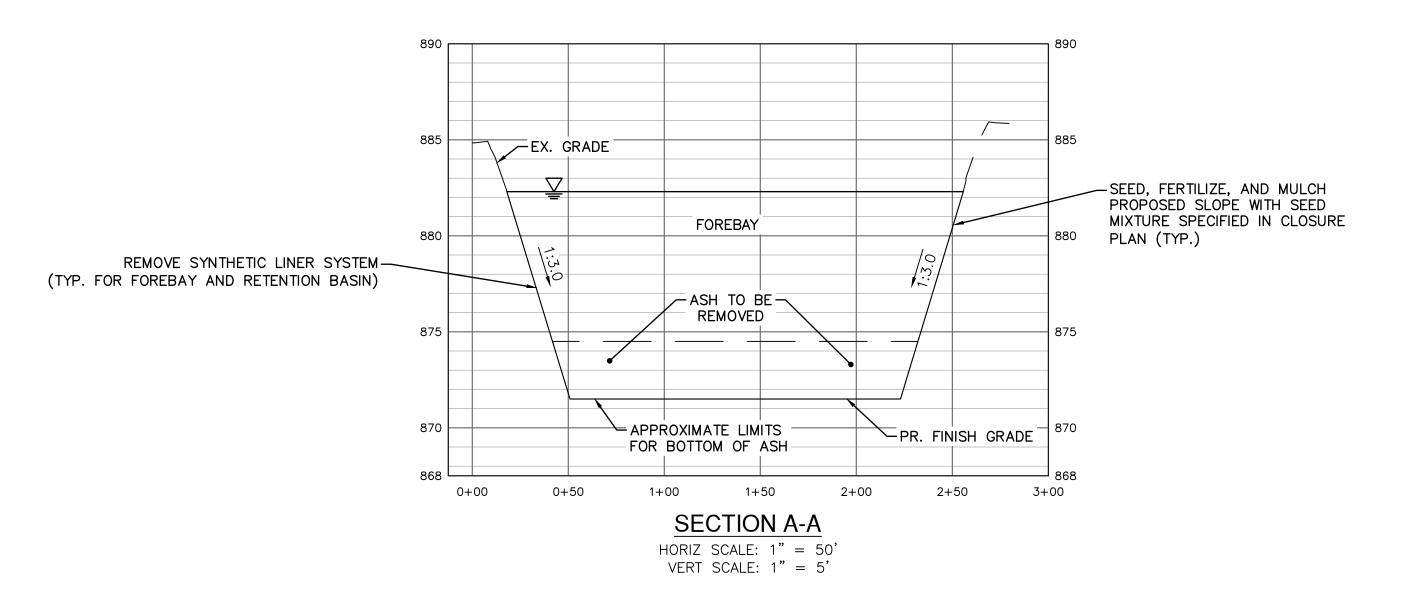
IMPOUNDMENT CLOSURE

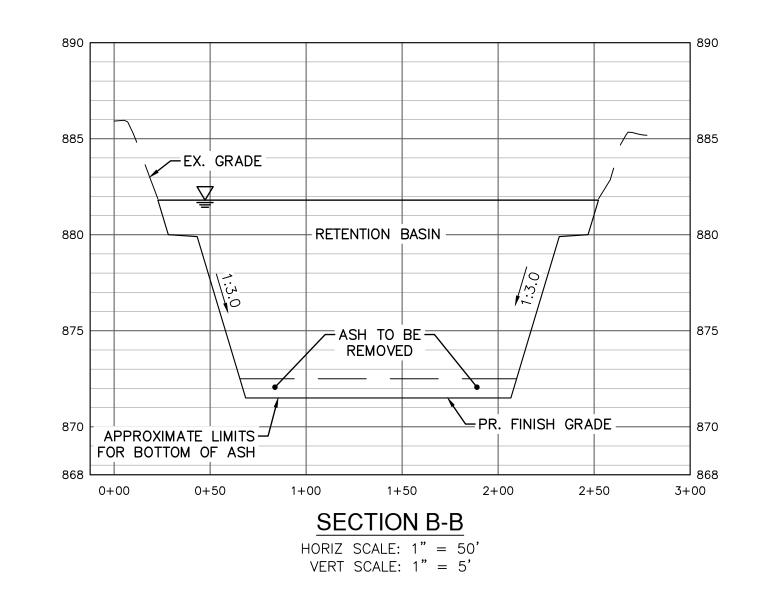
NTH PROJECT NO.: 73-180055	CAD FILE NAME: 180055-CLS
DESIGNED BY:	INCEP DATE: 12/19/2018
DRAWN BY: SLG	DRAWING SCALE: 1" = 100'
CHECKED BY: DRL	SUBMITTED DATE: 8/15/2019
SHEET TITLE:	

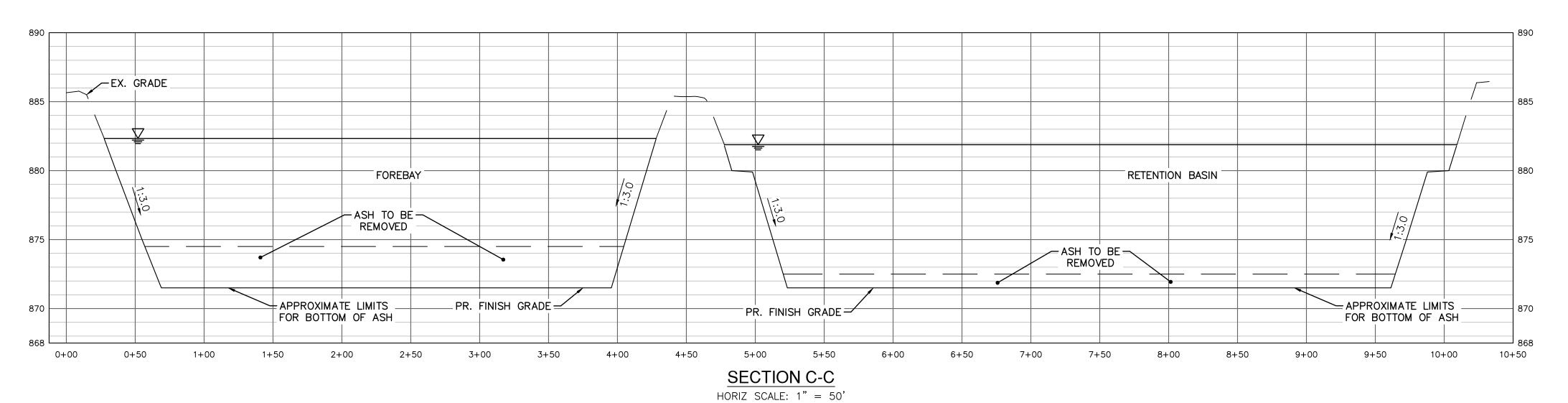
PROPOSED GRADING

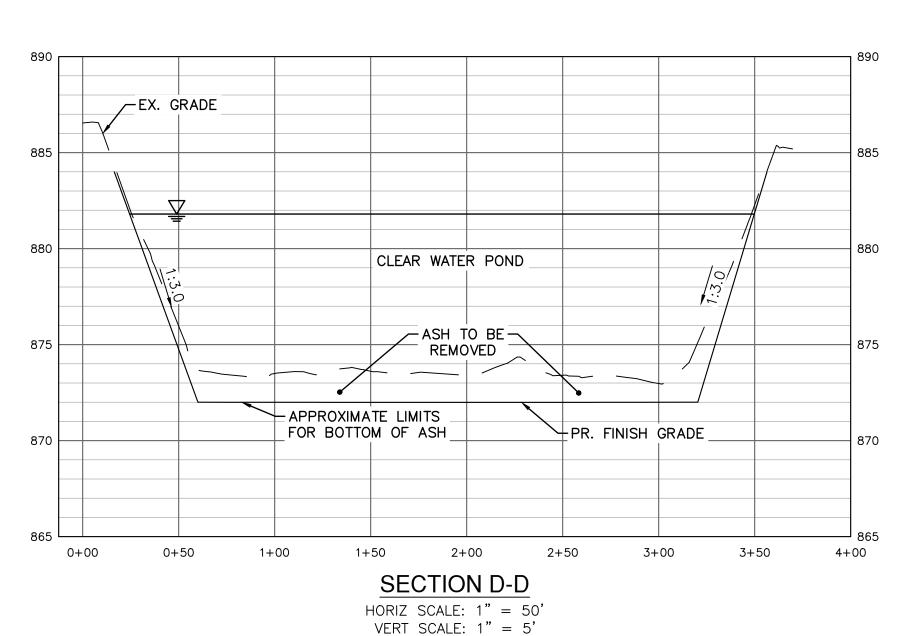
SHEET REFERENCE NUMBER:

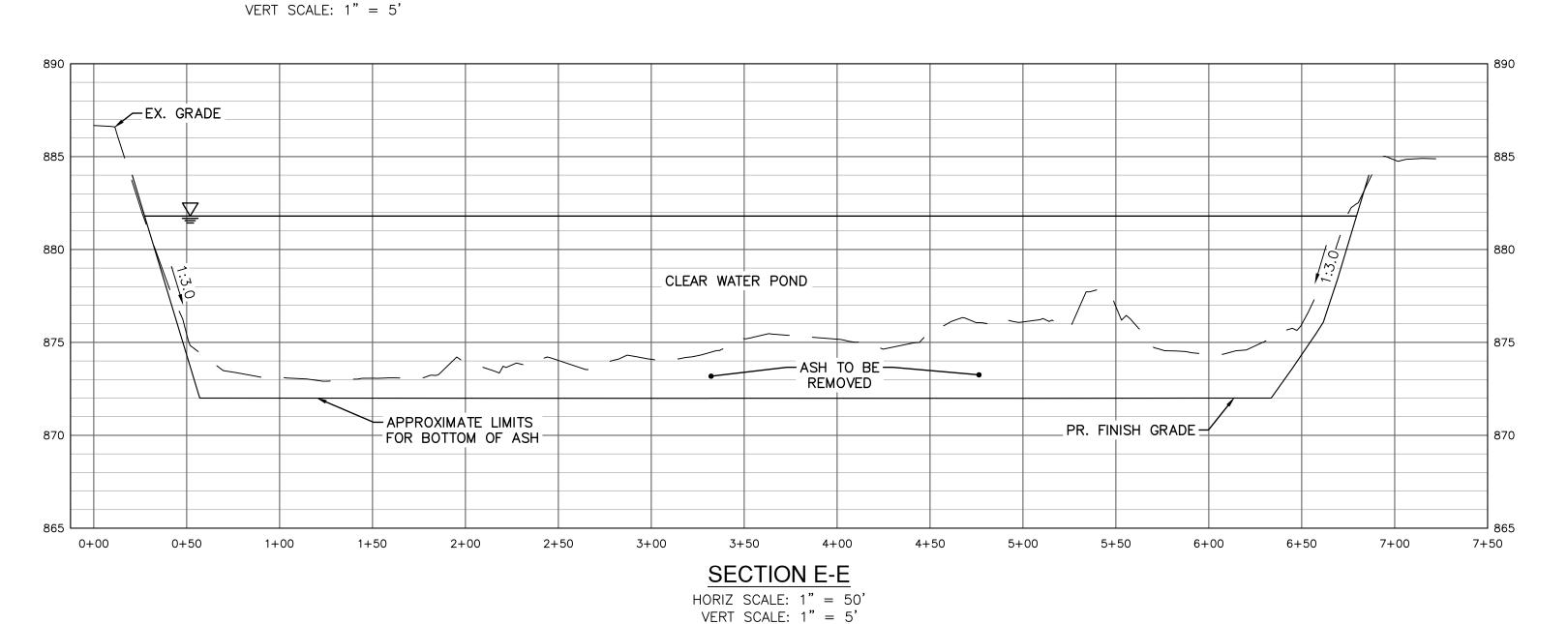
3













NOTES:

- EXISTING TOPOGRAPHIC SURVEY COMPLETED BY DRONEVIEW ON SEPTEMBER 26, 2018. VERTICAL DATUM IS IN NAVD 88.
- 2. NO POND BOTTOM SOUNDING WAS PERFORMED FOR THE FOREBAY AND RETENTION BASIN. ASH VOLUME ESTIMATED BASED ON REMOVAL EFFICIENCY OF PLANT HYDROBINS.
- 3. BOTTOM OF ASH LIMITS FOR FOREBAY AND RETENTION BASIN BASED ON INFORMATION PROVIDED IN THE CONSTRUCTION DOCUMENTATION REPORT FOR THE ASH IMPOUNDMENT RECONFIGURATION BY MAYOTTE DESIGN AND ENGINEERING, P.C., DATED MAY 2015.
- 4. BOTTOM OF ASH LIMITS FOR CLEAR WATER POND BASED ON HISTORICAL PLANT DRAWINGS 4848-183 "ASH POND STRUCTURES SHEET 1" AND 4848-184 "ASH POND STRUCTURES SHEET 2".

	SUBMITTAL		
REV	DESCRIPTION	DATE	B,

NTH Consultants, Ltd.

Infrastructure Engineering and

Environmental Services

248.553.6300

313.237.3900

517.484.6900

616.451.6270 216.334.4040

Northville, MI

Detroit, MI

Lansing, MI

Grand Rapids, MI

Cleveland, OH

ERICKSON STATION ASH IMPOUNDMENT CLOSURE

PROJECT LOCATION:

ERICKSON STATION LANSING, MICHIGAN

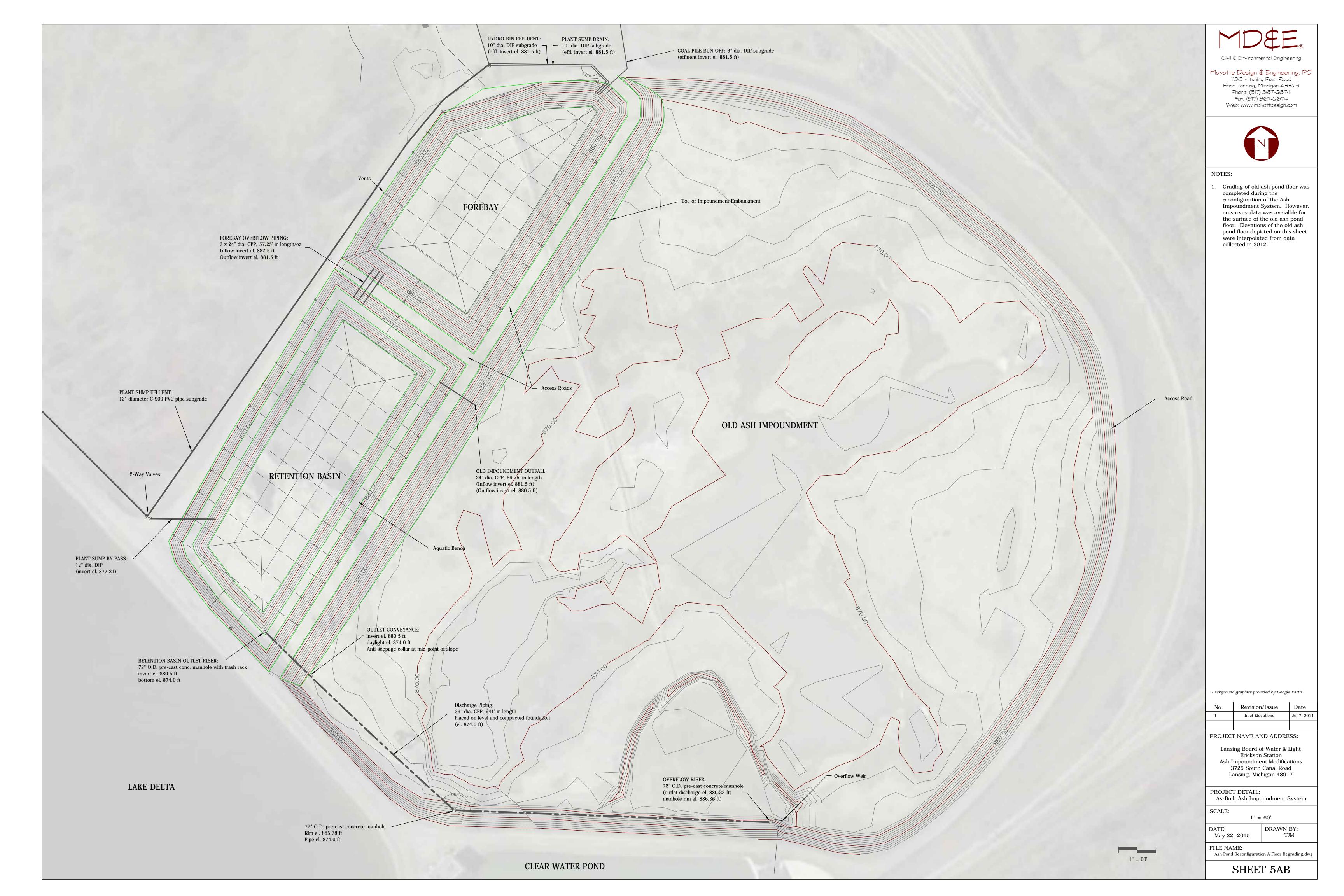
NTH PROJECT NO.:	CAD FILE NAME:
73-180055	180055-CLS
DESIGNED BY:	INCEP DATE:
SLG	12/19/2018
DRAWN BY:	DRAWING SCALE:
SLG	1" = 50'
CHECKED BY:	SUBMITTED DATE:
DRL	8/15/2019

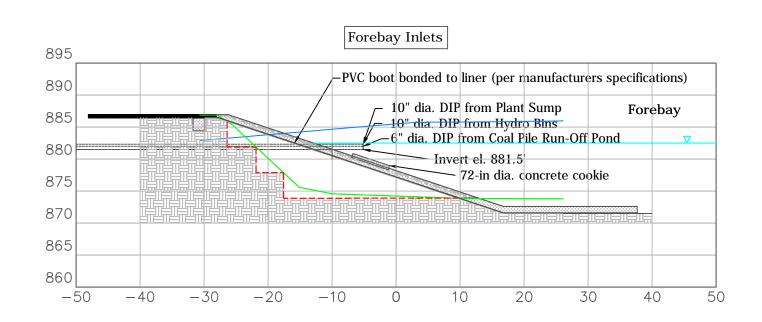
PROPOSED GRADING PROFILES

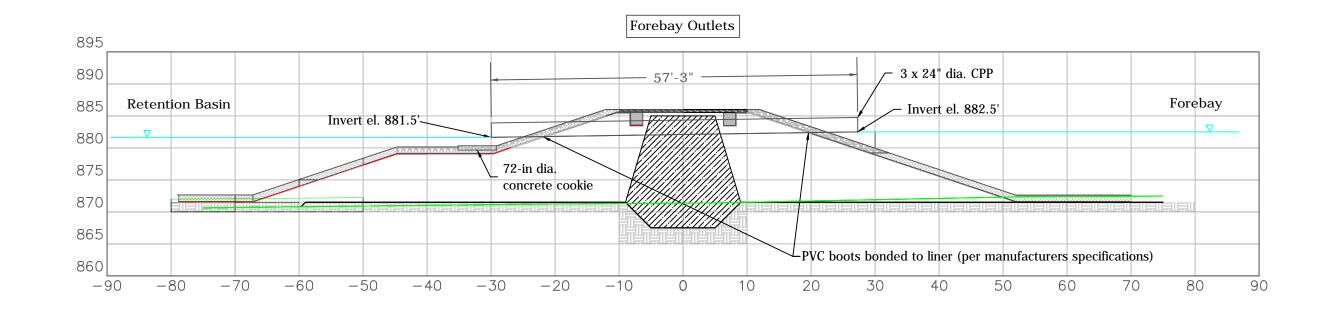
SHEET REFERENCE NUMBER:

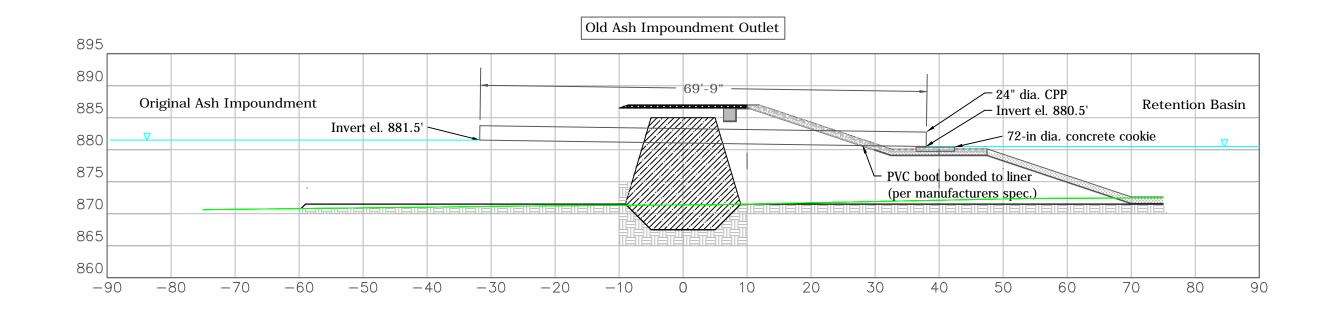
4

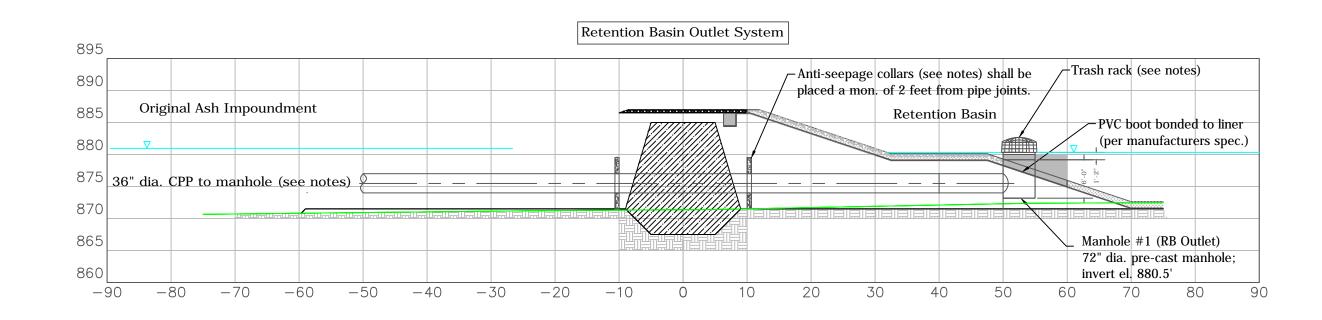
ATTACHMENT 6 AS-BUILT DRAWINGS FOR FORMER FOREBAY & FORMER RETENTION BASIN

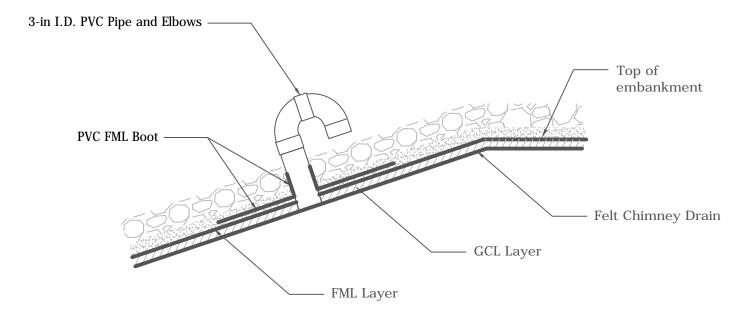




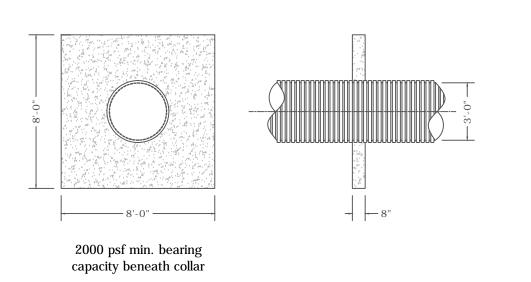




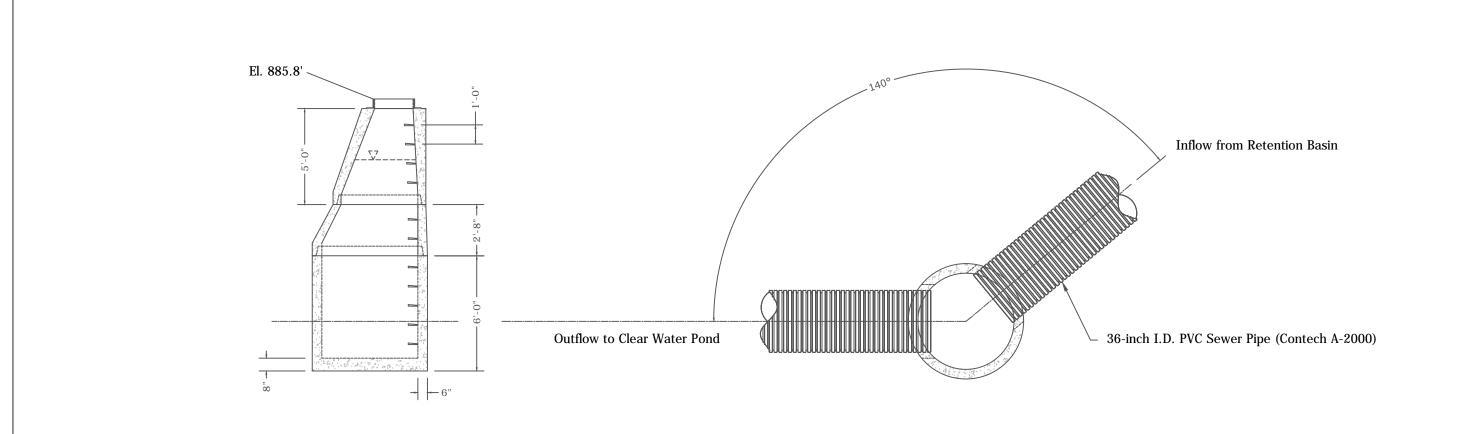




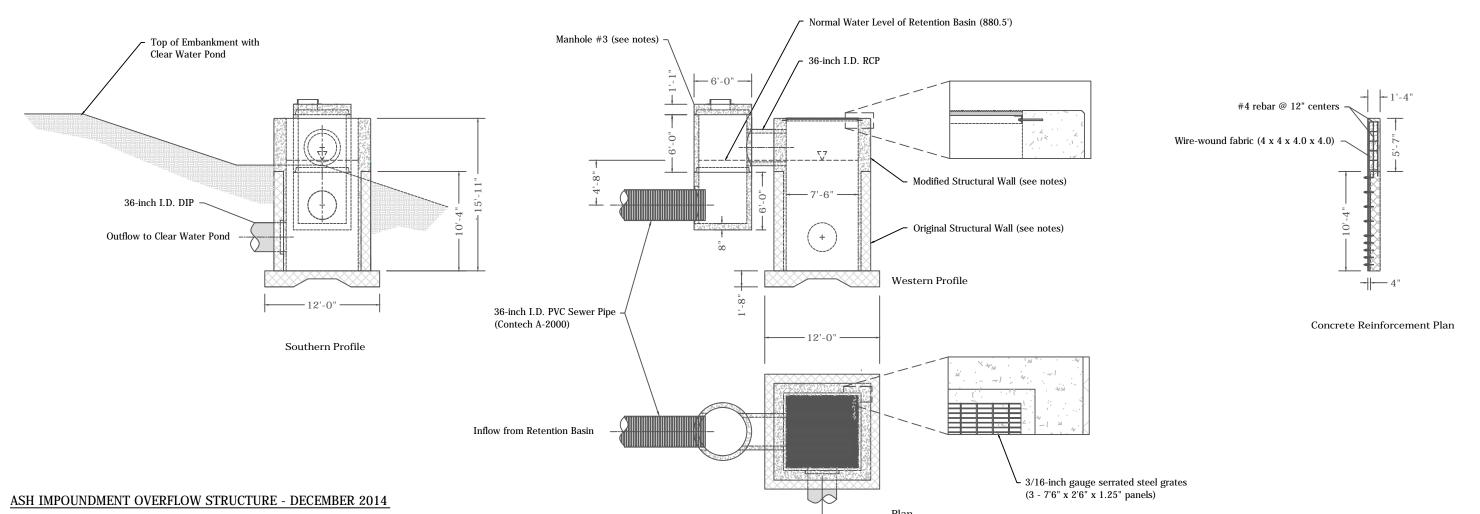
AIR/GAS VENT DETAIL



ANTI-SEEPAGE COLLARS



PRE-CAST MANHOLE #2





Civil & Environmental Engineering

Mayotte Design & Engineering, PC 1130 Hitching Post Road
East Lansing, Michigan 48823
Phone: (517) 367-2674
Fax: (517) 367-2674 Web: www.mayottdesign.com



- 1. All poured concrete is 3000 psi (28 day), unless noted otherwise.
- 2. Trash Rack: Contech Construction Products Inc. Round Series,
- . Air/Gas Vents are positioned at the perimeters of the Forebay and Retention Basins as depicted on SHEET 5AB.
- 4. Pre-cast manholes constructed of 4000 psi concrete (at 28 days).
- 5. Manholes designed for H-20 wheel

loading.

0.12 in sq/L.F.

- 6. Manholes constructed to conform to ASTM C-478 and MDOT
- specifications. Manhole concrete to reinforced to
- 8. Mahole shiplap joints sealed with butyl rubber gaskets.
- 9. PVC and concrete pipe sealed in manhole structures with
- cement/grout mixture. 10. Manhole covers and frames are
- Model 1040 from East Jordan Iron Works, Inc.
- 11. Dimensions for Anti-Seepage Collars are approximate.
- 12. Details of the original concrete and piping elements of the Overflow Weir are summarized on Ash Pound Structures SHEET 2, BWL Drawing No. 4848-184, approved Sept. 4, 1970.

Revision/Issue Date

PROJECT NAME AND ADDRESS:

Lansing Board of Water & Light Erickson Station Ash Impoundment Modifications 3725 South Canal Road Lansing, Michigan 48917

PROJECT DETAIL: As Noted

SCALE:

Varies DRAWN BY: May 22, 2015

FILE NAME: As-Built Profiles.dwg

SHEET 7AB

ATTACHMENT 7 CONSTRUCTION SPECIFICATIONS FOR FORMER FOREBAY & FORMER RETENTION BASIN

LANSING BOARD OF WATER & LIGHT

ERICKSON STATION ASH POND RECONFIGURATION

Foundation Preparation

1.0 **Scope**

- 1.1 The work consists of the preparation of a level foundation for the construction of the reconfigured ash pond (POND).
- 1.2 Earthfill is composed of natural earth materials that can be placed and compacted by construction equipment operated in a conventional manner.
- 1.3 Earth backfill is composed of natural arth material placed and compacted in confined spaces or adjacent to structures (including pipes) by hand tamping, manually directed power tampers or vibrating plates, o their equivalent.

2.0 Material

- 2.1 All fill material shall be obtain d from pre-approved borrow sources. The selection, ble ding, routing, and disposition of material in the arious fills shall be subject to approval by the SITE ENGINEER.
- 2.2 Fill materials shall contain no frozen soil, sod, brush, roots, or other erishable material. Rock particles larger than the maximum size specified for each type of fill shall be removed prior to compa tion of the fill.
- 2.3 The types of material used in the various fills shall be as listed and described in the specifications and drawings.

3.0 Pre-Construction Operations

- 3.1 Dewater the foundation area for the reconfigured ash pond (POND) depicted on Sheets 1 and 2:
 - 3.1.1 Furnish, install, operate and remove dewatering equipment necessary to drain and keep POND foundation area and associated excavations free of water under all circumstances.

- 3.1.2 Prevent surface water from flowing into excavations and promptly remove any accumulated water.
- 3.1.3 Where appropriate, dewatering equipment shall remain inplace until construction work below the ground water table is complete.
- 3.2 Relocate the temporary ash pond to area designated on Sheet
- 3.2 Re-route the plant sump effluent piping to connect with existing Hydro-Bin temporary discharge piping.
 - 3.2.1 To facilitate the connection to the Hydro-Bin effluent piping, the plant sump effluent plumbing must be redirected to the northeast along the north side of the access road, as depicted on Sheet 1.
 - 3.2.2 The sump piping is to penetrate the road/pond embankment at the appr ximate location identified on Sheet 1. The pipe penetration shall consist of a trench 4-6 feet deep and at least 36 inches wide. Compacted sand shall be placed ver the trench base to a depth of at least 6 inches. pe shall be placed over compacted sand base layer. Compacted sand shall be placed to a minimum pth of 6 inches above top of pipe. Earthfill deemed uitable by the engineer shall be backfilled compacted to the surface elevation of the embankment.

4.0 **Pond Foundation Preparation**

- 4.1 Except as ot erwise specified, the POND foundation area designated on Sheet 2 shall be graded to remove surface irregularities and to establish a level elevation of 871.5 feet NGVD.
 - 4.1.1 The foundation area shall be stripped to remove vegetation, coal ash and other unsuitable material. Strip topsoil, vegetation and other objectionable material to a minimum depth of 6 inches. Dispose residual ash. Stockpile clean topsoil in areas designated on Sheet 1 for potential use for subsequent construction activities.

- 4.1.2 Excavate soil in the Cut areas identified on Sheet 3 to an elevation of 871.5 feet NGVD.
- 4.1.3 Scrape 6 inches of pond footprint in the Fill areas identified on Sheet 3 areas to remove residual ash, verify foundation conditions and scarify ground surface to facilitate bond for backfill. Dispose residual ash. Stockpile excavated soil in areas designated on Sheet 1.
- 4.1.4 The SITE ENGINEER shall inspect and approve the structural competence of the exposed Cut and Fill surfaces prior to scarification or placement of any backfill.
- 4.1.5 Upon approval by SITE ENGINEER, Cut and Fill areas that are deemed competent to support compaction equipment shall be scarified to a depth of 2 inches and compacted to within 95% of the maximum dry density of the foundation soils, as determined by the SITE ENGINEER.
- 4.1.6 Place backfill in the Fill areas designated on Sheet 3 to achieve a level surface elevation of 871.5 feet NGVD. Initial lifts of backfill shall be shall be placed within Fill areas of lowest elevations. Backfill lifts shall be no greater than 8 inches in thickness uncompacted and must be parallel to the target foundation surface. Backfill shall be compacted to within 95% of the maximum dry density of the backfill, as determined by the SITE ENGINEER. Backfill layers shall be continuously manipulated to provide uniform layers approximately parallel to the finished grade.
- 4.1.7 After stripping and cut and fill operations have resulted in a contiguous level surface, the foundation shall be scarified parallel to the axis of the placement of fill material or otherwise acceptably scored and loosened to a minimum depth of 2 inches. The moisture content of the loosened material shall be controlled as specified for the backfill, and the surface material of the foundation shall be compacted and bonded with the first layer of backfill to within 95% of the maximum dry density of the backfill, as determined by the SITE ENGINEER.

- 4.1.8 Excavate cut-off trenches along the alignments and to the specifications designated on Sheet 2. Stockpile acceptable excavated materials in areas designated on Sheet 1.
- 4.1.9 Ensure that cut-off trenches are adequately dewatered to facilitate placement and compaction of designated backfill to within 95% of the maximum dry density of the material, as determined by SITE ENGINEER.

ATTACHMENT 8 2025 AS-BUILT DRAWINGS FOR IMPOUNDMENT CLOSURE

Contract Drawings For

Lansing Board of Water & Light

INDEX OF DRAWINGS

FINAL GRADING CROSS SECTIONS FINAL GRADING CROSS SECTIONS

Former Erickson Power Station Ash Impoundments Closure

Issued for As-Built

Project No. 10338772

Lansing, Michigan July 2025

THIS DOCUMENT WAS ORGINALLY ISSUED AND SEALED TERRY BRYCE BURKETT, LICENSE NO.

KEY PLAN:

ISSUED FOR CONSTRUCTION

MILLETT HWY



DATE:	07/09/2025	DWG BY:	C. ABBOTT
CHK BY:	B. BURKETT	APPR BY:	B. BURKETT
PROJ NO:	10338772	STATUS:	AS-BUILT

POWER STATION ASH

ERICKSON

DISCIPLINE: CIVIL

BWL DRAWING NUMBER:

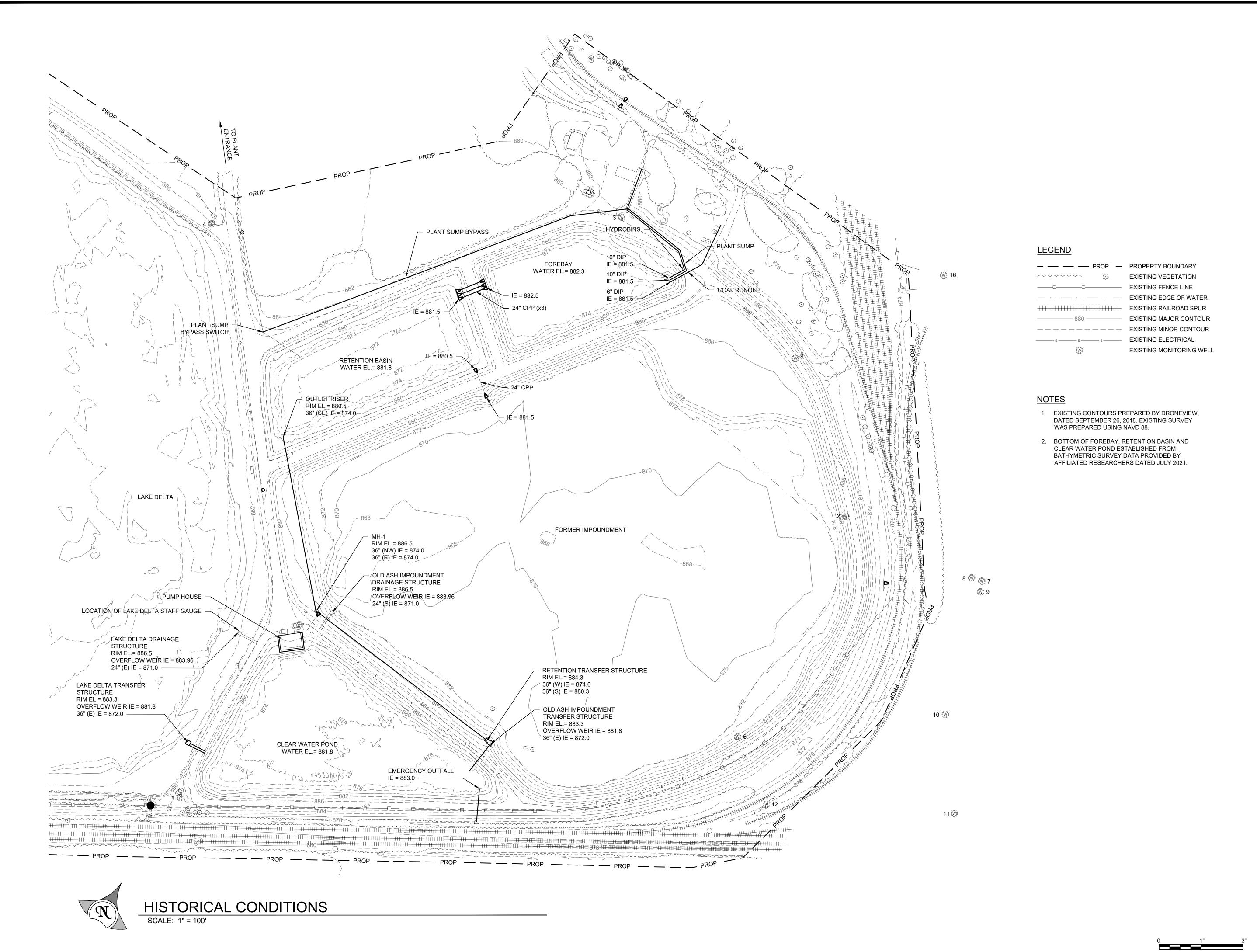
G-1000

REVISION:

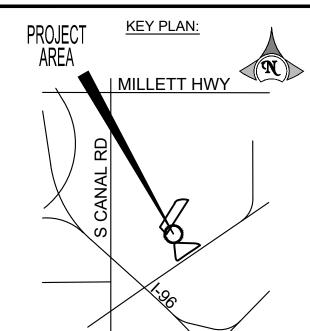


VICINITY MAP

6201066757 ON JANUARY 31, 2023. PROJECT NAME:
FORMER ERICKSON IMPOUNDMENTS CLOSURE **COVER SHEET** STR/AREA: GENERAL SITE (ALL SHEETS)







	REVISIONS:						
REV.	DESCRIPTION	BY	СНК	DATE			
0	ISSUED FOR BID	BB	LZ	10-12-2022			
1	ISSUED FOR CONSTRUCTION	BB	LZ	01-31-2023			
2	AS-BUILT	BB	LZ	07-09-2025			
			i l	1			

FJS

DATE:	07/09/2025	DWG BY:	C. ABBOTT
CHK BY:	B. BURKETT	APPR BY:	B. BURKETT
PROJ NO:	10338772	STATUS:	AS-BUILT
DDU IECT NAME	,		

FORMER ERICKSON

POWER STATION ASH
IMPOUNDMENTS CLOSURE

DRAWING TITLE:

HISTORICAL

CONDITIONS

SITE: ERICKSON

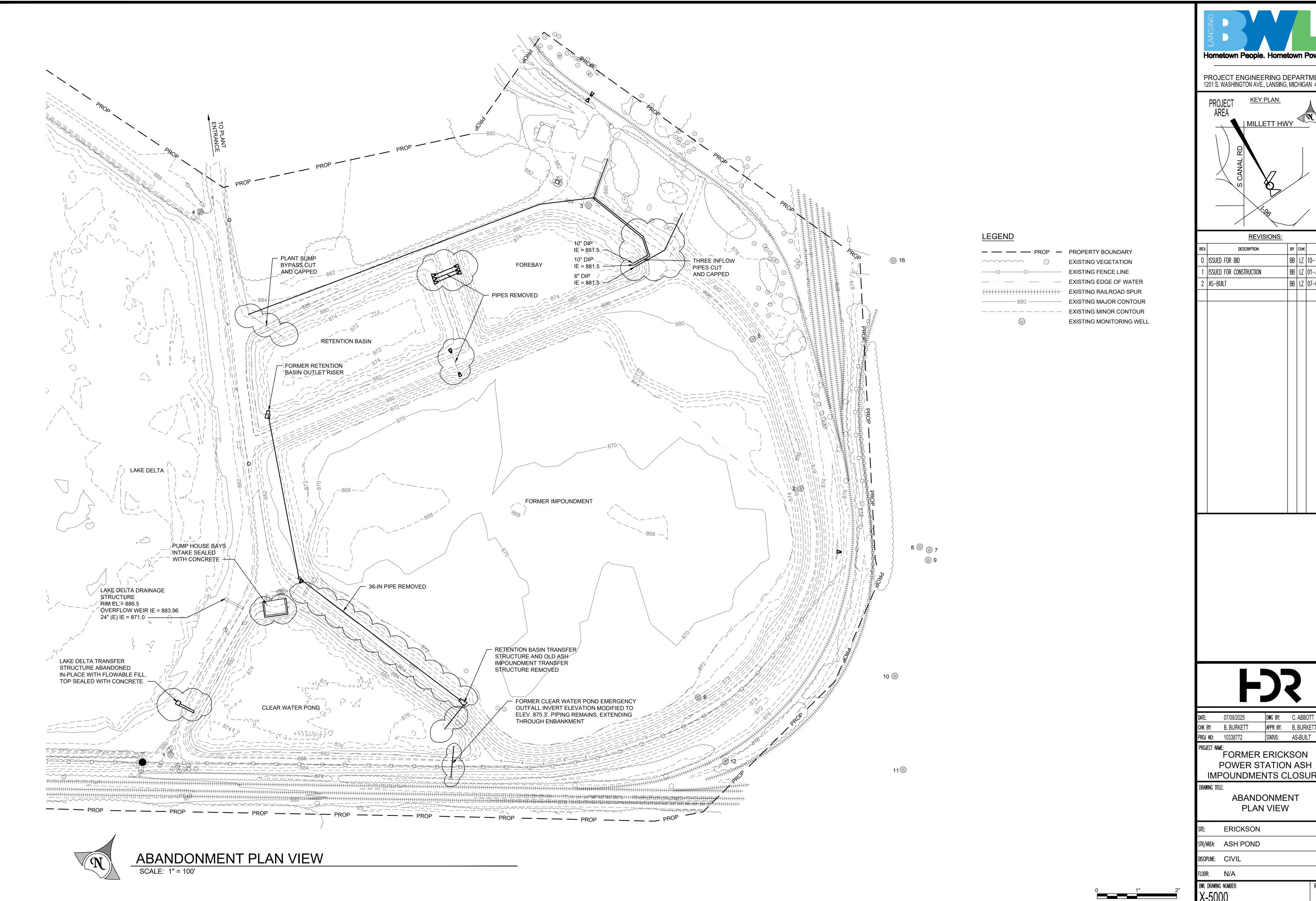
STR/AREA: ASH POND

DISCIPLINE: CIVIL

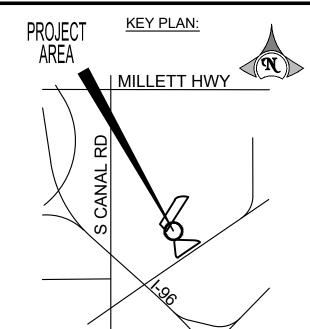
FLOOR: N/A

BWL DRAWING NUMBER: REVISION:

E-3000







	•					
	REVISIONS:					
REV.	DESCRIPTION	BY	СНК	DATE		
0	ISSUED FOR BID	BB	LZ	10-12-2022		
1	ISSUED FOR CONSTRUCTION	BB	LZ	01-31-2023		
2	AS-BUILT	BB	LZ	07-09-2025		

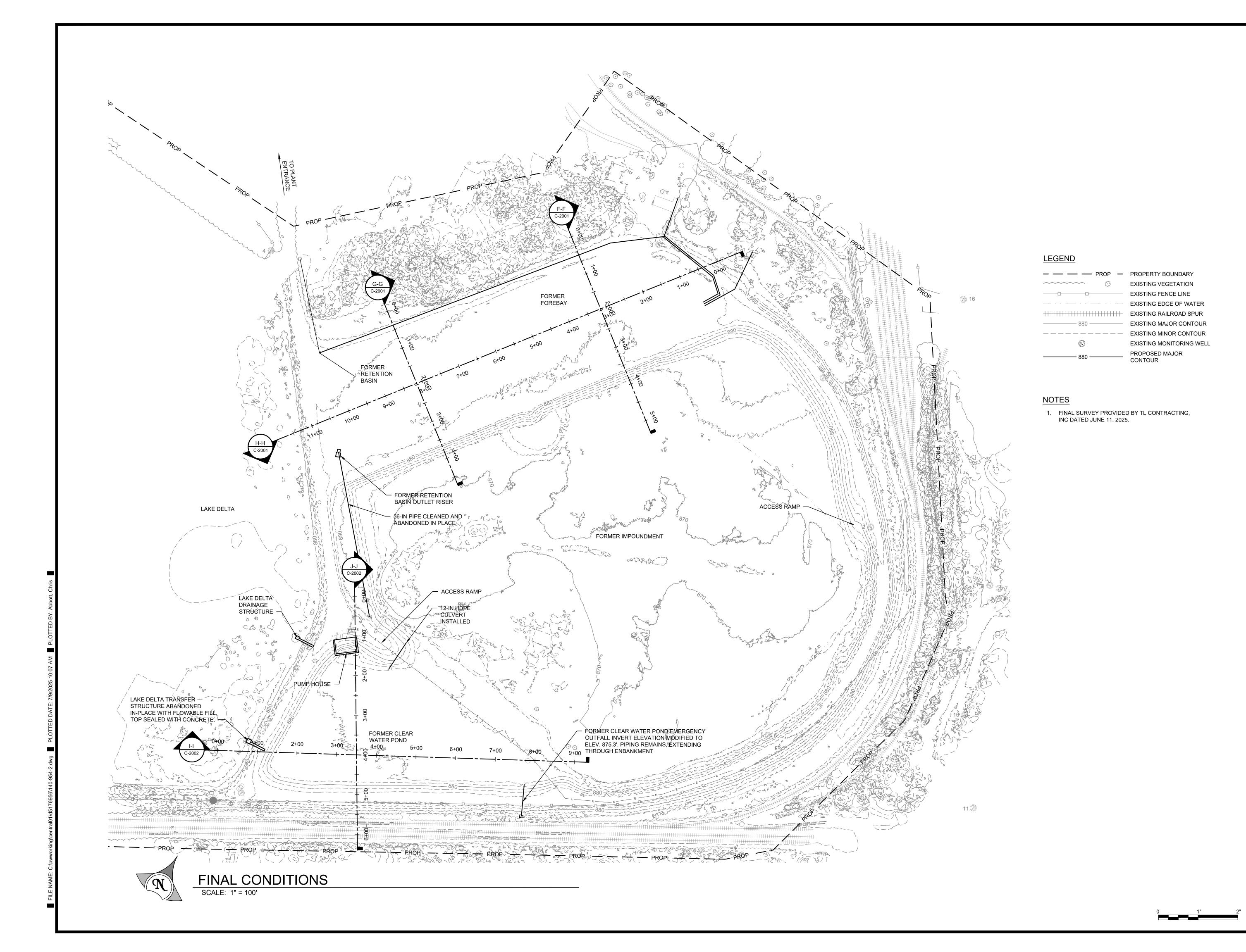


D/IIL.	0110012020	יום טווט.	O. ADDOTT
CHK BY:	B. BURKETT	APPR BY:	B. BURKETT
PROJ NO:	10338772	STATUS:	AS-BUILT
PROJECT NAME	•		

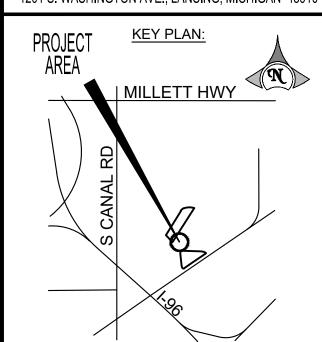
FORMER ERICKSON POWER STATION ASH IMPOUNDMENTS CLOSURE

ABANDONMENT **PLAN VIEW**

SITE:	ERICKSON	
STR/AREA:	ASH POND	
DISCIPLINE:	CIVIL	
FLOOR:	N/A	
BWL DRAWING	NUMBER:	REVISION







	REVISIONS:					
REV.	DESCRIPTION	BY	СНК	DATE		
0	ISSUED FOR BID	BB	LZ	10-12-2022		
1	ISSUED FOR CONSTRUCTION	BB	LZ	01-31-2023		
2	AS-BUILT	BB	LZ	07-09-2025		

FJS

DATE:	07/09/2025	DWG BY:	C. ABBOTT
CHK BY:	B. BURKETT	APPR BY:	B. BURKETT
PROJ NO:	10338772	STATUS:	AS-BUILT

PROJECT NAME:
FORMER ERICKSON
POWER STATION ASH
IMPOUNDMENTS CLOSURE

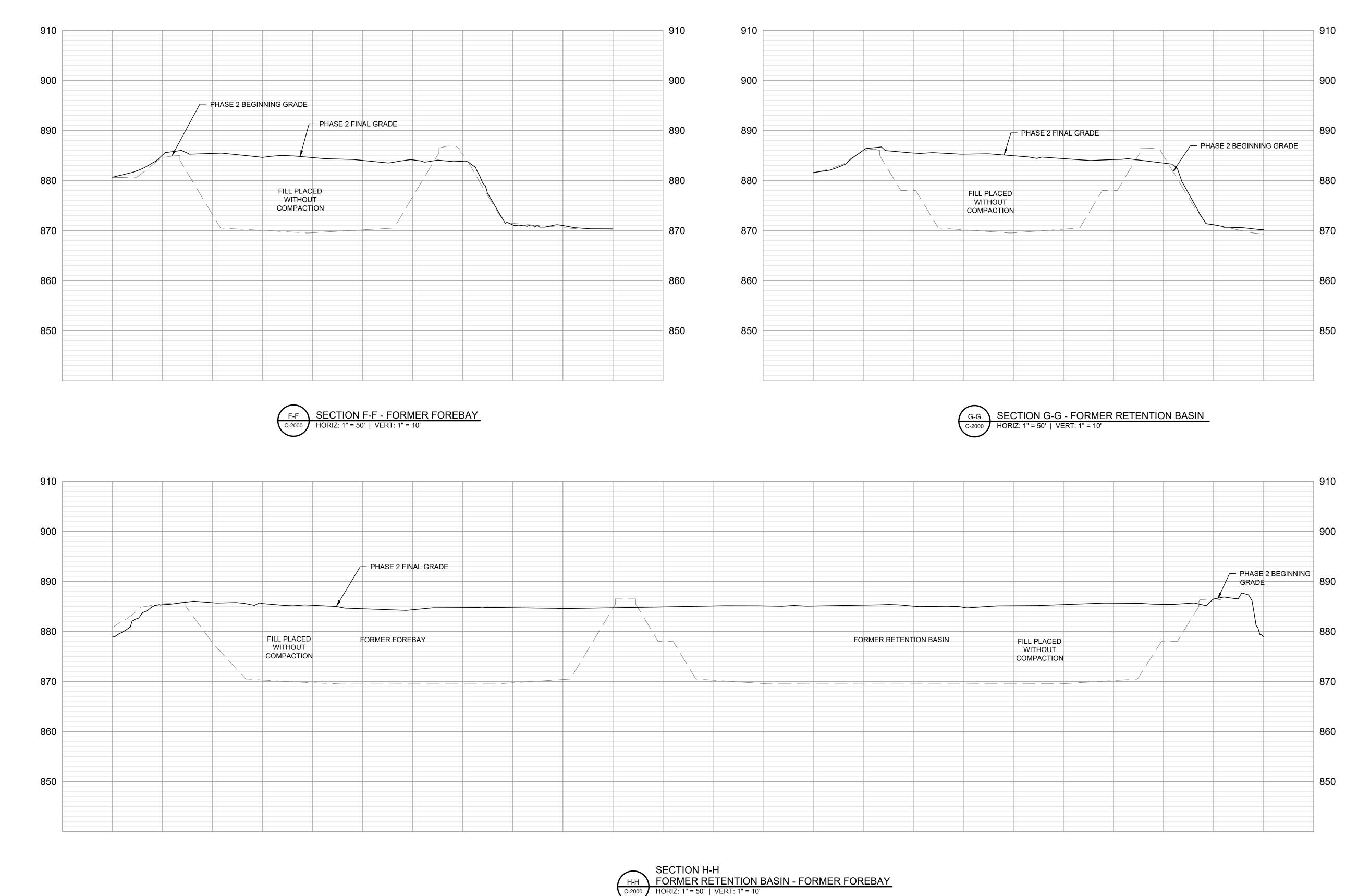
FINAL CONDITIONS

SITE:	ERICKSON
STR/ARFA	ASH POND

DISCIPLINE: CIVIL SITE GRADING

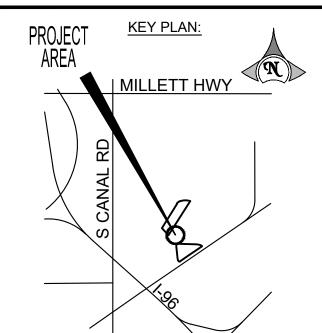
FLOOR: N/A
BWL DRAWING NUMBER:

BWL DRAWING NUMBER: REVISION: 2









	REVISIONS:				
REV.	DESCRIPTION	BY	СНК	DATE	
0	ISSUED FOR BID	BB	LZ	10-12-2022	
1	ISSUED FOR CONSTRUCTION	BB	LZ	01-31-2023	
2	AS-BUILT	BB	LZ	07-09-2025	

DATE:	07/09/2025	DWG BY:	C. ABBOTT
CHK BY:	B. BURKETT	APPR BY:	B. BURKETT
PROJ NO:	10338772	STATUS:	AS-BUILT

PROJECT NAME:
FORMER ERICKSON POWER STATION ASH IMPOUNDMENTS CLOSURE

> FINAL GRADING **CROSS SECTIONS**

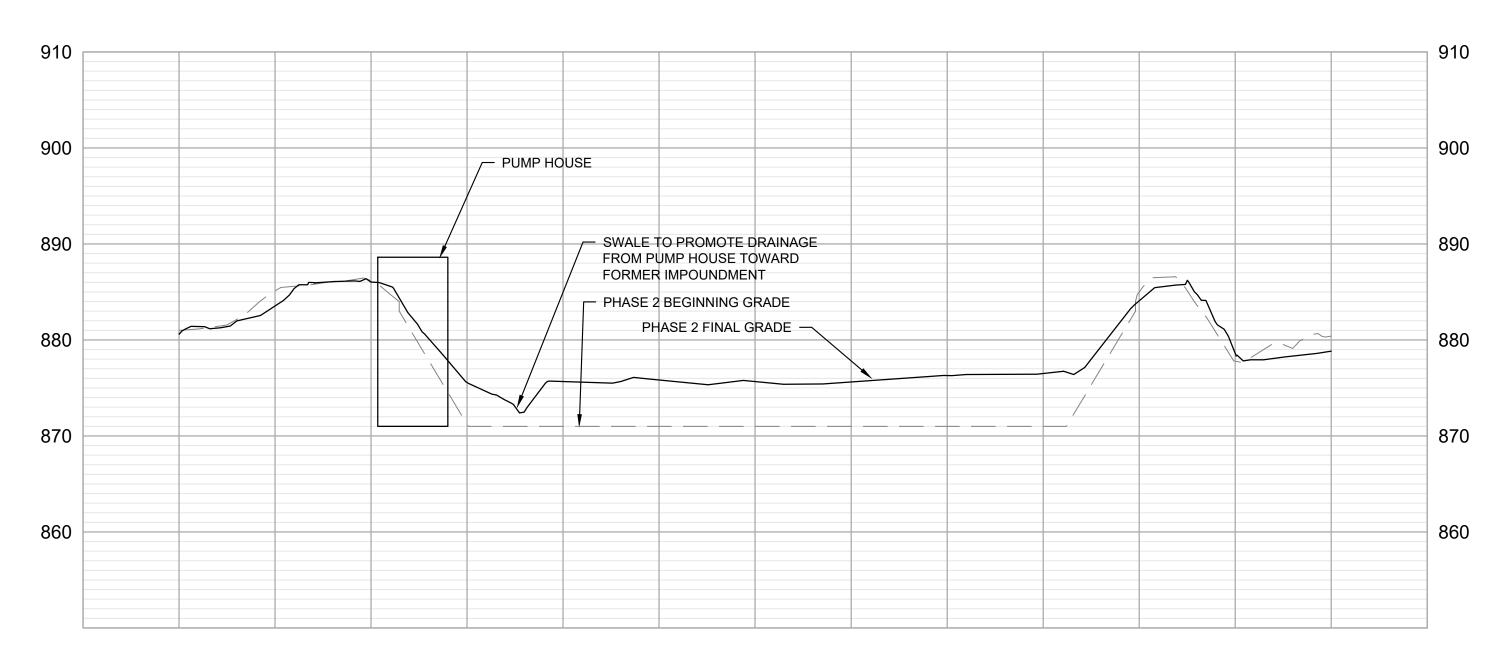
ERICKSON

STR/AREA: ASH POND DISCIPLINE: CIVIL SITE GRADING

FLOOR: N/A

REVISION: BWL DRAWING NUMBER: C-2001

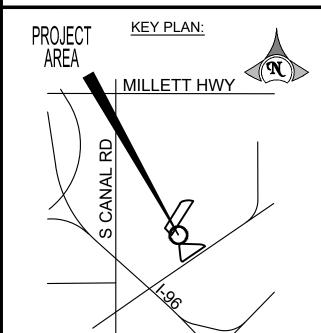




SECTION J-J FORMER CLEAR WATER POND HORIZ: 1" = 50' | VERT: 1" = 10'



PROJECT ENGINEERING DEPARTMENT 1201 S. WASHINGTON AVE., LANSING, MICHIGAN 48910



	REVISIONS:					
REV.	DESCRIPTION	BY	СНК	DATE		
0	ISSUED FOR BID	BB	LZ	10-12-2022		
1	ISSUED FOR CONSTRUCTION	BB	LZ	01-31-2023		
2	AS-BUILT	BB	LZ	07-09-2025		

DATE:	07/09/2025	DWG BY:	C. ABBOTT
CHK BY:	B. BURKETT	APPR BY:	B. BURKETT
PROJ NO:	10338772	STATUS:	AS-BUILT
DRUIECT NAME	•		

PROJECT NAME:
FORMER ERICKSON POWER STATION ASH IMPOUNDMENTS CLOSURE

> FINAL GRADING **CROSS SECTIONS**

ERICKSON

STR/AREA: ASH POND

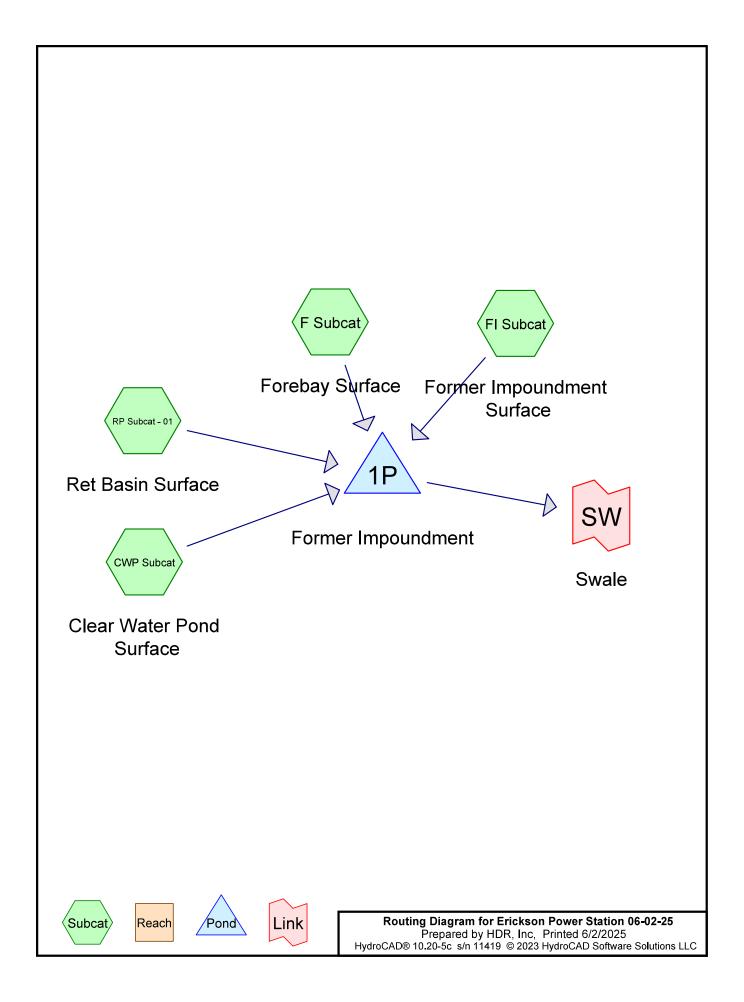
DISCIPLINE: CIVIL SITE GRADING

FLOOR: N/A

BWL DRAWING NUMBER: C-2002

REVISION:

ATTACHMENT 9 2025 CAPACITY CALCULATIONS FOR FORMER IMPOUNDMENT SYSTEM



Prepared by HDR, Inc HydroCAD® 10.20-5c s/n 11419 © 2023 HydroCAD Software Solutions LLC Printed 6/2/2025 Page 2

Project Notes

For drainage areas:

The Former Forebay receives water from the Forebay surface area

The Former Retention Pond receives water from Retention Pond surface area

The Former Clear Wastewater Pond receives water from Clear Water Pond surafce area

The Former Impoundment receives water from the Former Impoundment surface area

The swale receives water from the Former Clear Water Pond outfall (does not spill over in 100-yr event)

Prepared by HDR, Inc HydroCAD® 10.20-5c s/n 11419 © 2023 HydroCAD Software Solutions LLC

Printed 6/2/2025 Page 3

Area Listing (all nodes)

Are	ea CN	Description
(acre	s)	(subcatchment-numbers)
31.2	49 61	>75% Grass cover, Good, HSG B (CWP Subcat, F Subcat, FI Subcat, RP Subcat - 01)
6.1	30 98	Impoundment (FI Subcat)
37.4	29 67	TOTAL AREA

Prepared by HDR, Inc HydroCAD® 10.20-5c s/n 11419 © 2023 HydroCAD Software Solutions LLC

Printed 6/2/2025 Page 4

Soil Listing (all nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
0.000	HSG A	
31.249	HSG B	CWP Subcat, F Subcat, FI Subcat, RP Subcat - 01
0.000	HSG C	
0.000	HSG D	
6.180	Other	FI Subcat
37.429		TOTAL AREA

Prepared by HDR, Inc HydroCAD® 10.20-5c s/n 11419 © 2023 HydroCAD Software Solutions LLC

Printed 6/2/2025

Page 5

Ground Covers (all nodes)

HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
0.000	31.249	0.000	0.000	0.000	31.249	>75% Grass cover, Good	CWP Subcat, F Subcat, FI Subcat, RP Subcat -
0.000	0.000	0.000	0.000	6.180	6.180	Impoundment	FI Subcat
0.000	31.249	0.000	0.000	6.180	37.429	TOTAL AREA	

Prepared by HDR, Inc HydroCAD® 10.20-5c s/n 11419 © 2023 HydroCAD Software Solutions LLC

Printed 6/2/2025

Page 6

Pipe Listing (all nodes)

Line#	Node	In-Invert	Out-Invert	Length	Slope	n	Width	Diam/Height	Inside-Fill	Node
	Number	(feet)	(feet)	(feet)	(ft/ft)		(inches)	(inches)	(inches)	Name
1	1P	875.30	875.30	50.0	0.0000	0.011	0.0	36.0	0.0	

Type II 24-hr 100- yr 24-hr Rainfall=5.38"

Erickson Power Station 06-02-25

Prepared by HDR, Inc

HydroCAD® 10.20-5c s/n 11419 © 2023 HydroCAD Software Solutions LLC

Printed 6/2/2025

Page 7

Time span=0.00-24.00 hrs, dt=0.01 hrs, 2401 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

SubcatchmentCWP Subcat: Clear Water Runoff Area=5.739 ac 0.00% Impervious Runoff Depth>1.59" Flow Length=100' Slope=0.0200 '/' Tc=16.4 min CN=61 Runoff=10.74 cfs 0.762 af

SubcatchmentF Subcat: Forebay Surface Runoff Area=2.760 ac 0.00% Impervious Runoff Depth>1.59" Flow Length=100' Slope=0.0200 '/' Tc=16.4 min CN=61 Runoff=5.16 cfs 0.366 af

SubcatchmentFl Subcat: Former Runoff Area=25.200 ac 24.52% Impervious Runoff Depth>2.31" Flow Length=115' Slope=0.0200 '/' Tc=16.8 min CN=70 Runoff=70.98 cfs 4.853 af

SubcatchmentRP Subcat - 01: Ret Basin Runoff Area=3.730 ac 0.00% Impervious Runoff Depth>1.59" Flow Length=100' Slope=0.0200 '/' Tc=16.4 min CN=61 Runoff=6.98 cfs 0.495 af

Pond 1P: Former Impoundment Peak Elev=869.06' Storage=6.476 af Inflow=93.85 cfs 6.476 af 36.0" Round Culvert n=0.011 L=50.0' S=0.0000 '/' Outflow=0.00 cfs 0.000 af

Link SW: Swale

Inflow=0.00 cfs 0.000 af

Primary=0.00 cfs 0.000 af

Total Runoff Area = 37.429 ac Runoff Volume = 6.476 af Average Runoff Depth = 2.08" 83.49% Pervious = 31.249 ac 16.51% Impervious = 6.180 ac

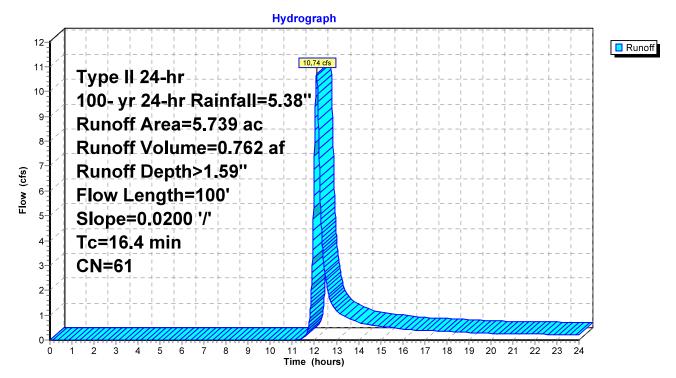
Summary for Subcatchment CWP Subcat: Clear Water Pond Surface

Runoff = 10.74 cfs @ 12.10 hrs, Volume= 0.762 af, Depth> 1.59" Routed to Pond 1P : Former Impoundment

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type II 24-hr 100- yr 24-hr Rainfall=5.38"

Area	(ac) C	N Des	cription					
5.	739 6	31 >75°	% Grass co	over, Good	, HSG B			
5.	5.739 100.00% Pervious Area							
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
16.4	100	0.0200	0.10		Sheet Flow, Sheet Flow Grass: Dense n= 0.240 P2= 2.42"			

Subcatchment CWP Subcat: Clear Water Pond Surface



Summary for Subcatchment F Subcat: Forebay Surface

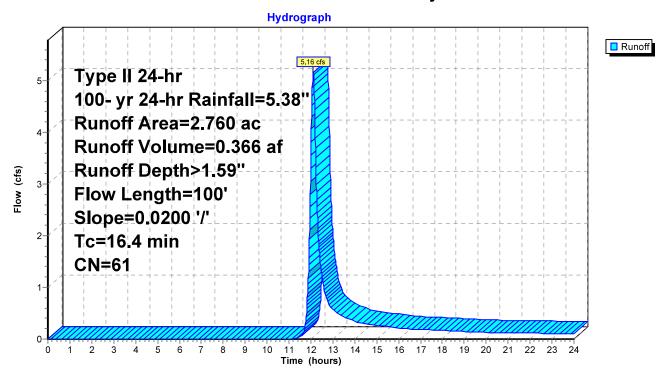
Runoff = 5.16 cfs @ 12.10 hrs, Volume= 0.366 af, Depth> 1.59"

Routed to Pond 1P: Former Impoundment

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type II 24-hr 100- yr 24-hr Rainfall=5.38"

Area	(ac) C	N Desc	cription						
2	.760 6	S1 >75%	% Grass c	over, Good	, HSG B				
2	2.760 100.00% Pervious Area								
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
16.4	100	0.0200	0.10		Sheet Flow, Forebay Surface Grass: Dense n= 0.240 P2= 2.42"				

Subcatchment F Subcat: Forebay Surface



Summary for Subcatchment FI Subcat: Former Impoundment Surface

Runoff = 70.98 cfs @ 12.10 hrs, Volume= 4

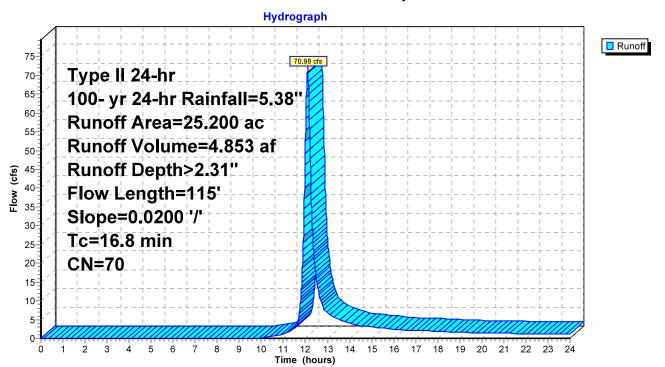
4.853 af, Depth> 2.31"

Routed to Pond 1P: Former Impoundment

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type II 24-hr 100- yr 24-hr Rainfall=5.38"

	Area	(ac)	CN	Desc	cription			
*	6.	180	98	Impo	undment			
	19.	020	61	>75%	√ Grass co	over, Good	, HSG B	
25.200 70 Weighted Average								
	19.	020		75.4	8% Pervio	us Area		
	6.	180		24.5	2% Imperv	∕ious Area		
	Tc (min)	Length (feet		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
	0.4	15	5		0.63		Direct Entry, OAI Subcat	
	16.4	100	0.	0200	0.10		Sheet Flow, Sheet Flow	
_							Grass: Dense n= 0.240 P2= 2.42"	
	16.8	115	5 To	otal				

Subcatchment FI Subcat: Former Impoundment Surface



Summary for Subcatchment RP Subcat - 01: Ret Basin Surface

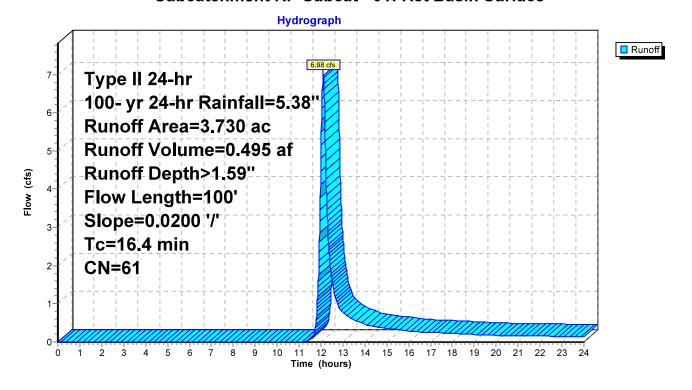
Runoff = 6.98 cfs @ 12.10 hrs, Volume= 0.495 af, Depth> 1.59" Routed to Pond 1P : Former Impoundment

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type II 24-hr 100- yr 24-hr Rainfall=5.38"

_	Area	(ac) C	N Des	cription		
	3.	730 6	61 >75°	% Grass c	over, Good	H, HSG B
	3.	730	100.	00% Pervi	ous Area	
	Тс	Length	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
_	16.4	100	0.0200	0.10		Sheet Flow Retention Basin - Sheet Flow

Subcatchment RP Subcat - 01: Ret Basin Surface

Grass: Dense n= 0.240 P2= 2.42"



Prepared by HDR, Inc.

Printed 6/2/2025

HydroCAD® 10.20-5c s/n 11419 © 2023 HydroCAD Software Solutions LLC

<u>Page 12</u>

Summary for Pond 1P: Former Impoundment

Inflow Area = 37.429 ac, 16.51% Impervious, Inflow Depth > 2.08" for 100- yr 24-hr event

Inflow = 93.85 cfs @ 12.10 hrs, Volume= 6.476 af

Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Primary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routed to Link SW: Swale

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 869.06' @ 24.00 hrs Surf.Area= 6.152 ac Storage= 6.476 af

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Center-of-Mass det. time= (not calculated: no outflow)

Volume	Invert	Avail.Storage	Storage Description
#1	868.00'	122.463 af	Custom Stage Data (Prismatic)Listed below (Recalc)

re-feet)
0.000
12.301
23.358
41.012
81.083
101.773
122.463

Device	Routing	Invert	Outlet Devices
#1	Primary	875.30'	36.0" Round Culvert

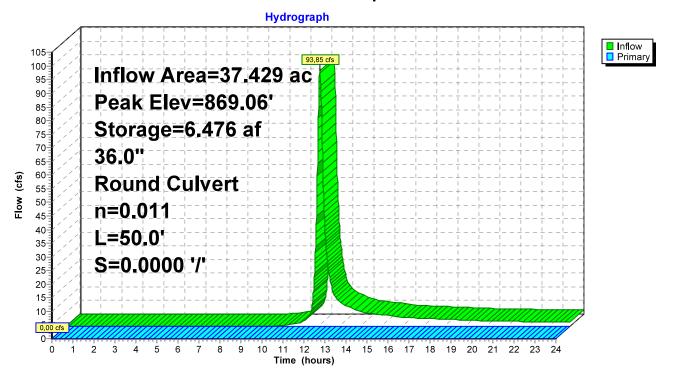
L= 50.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 875.30' / 875.30' S= 0.0000 '/' Cc= 0.900 n= 0.011 Concrete pipe, straight & clean, Flow Area= 7.07 sf

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=868.00' (Free Discharge) 1=Culvert (Controls 0.00 cfs)

HydroCAD® 10.20-5c s/n 11419 © 2023 HydroCAD Software Solutions LLC

Page 13

Pond 1P: Former Impoundment



Summary for Link SW: Swale

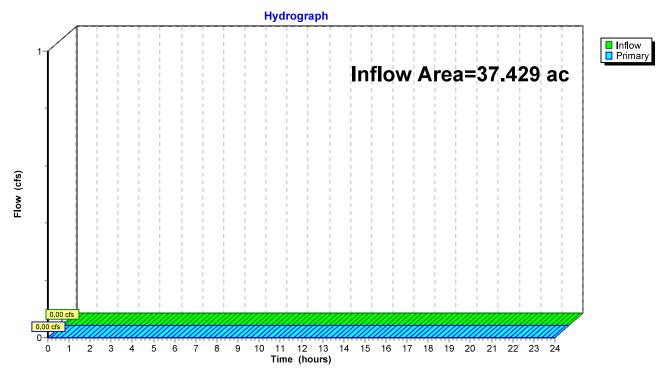
Inflow Area = 37.429 ac, 16.51% Impervious, Inflow Depth = 0.00" for 100- yr 24-hr event

Inflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Primary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

Link SW: Swale



ATTACHMENT 10 TYPICAL BWL WEEKLY INSPECTION REPORT

IRWI - WFFKLY INSPECTION REPORT - CCR SURFACE IMPOUNDMENT SYSTEM

Name: ROBERT L. ALEN W	Veather: SUNNX 43	Q						
	ite Conditions:			_				
If you answer "Yes	" to any of the following questions, describe an	d call E	Enviro	nmental Serv				
I. SURFACE IMPOUNDMENT	and the state of t		manner and	rebay	No. of Concession, Name of Street, or other Persons, Name of Street, or ot	ring to a very common.	ion Basin	Clearwater Pond
	cription	Yes	No	Not Visible	Yes	No	Not Visible	Yes No Not Visible
Is there any erosion around the impoundment?		X				X	X	
2. Is there excessive CCR (ash) build-up above the water su	ırface?		X				X	X
II. CREST								
Forebay	Retention Basin			La Carrier and Carrier	Z. L. L. L		earwater Pond	
1. Describe vegetation on the crest: Sparse Good cover Overgrown (taller than 6-inches) Rip Rap Gravel Other (describe):	1. Describe vegetation on the crest: Sparse Good cover Overgrown 6-inches) Rip Rap Gravel Other (des	· ·		1. Describe von Sparse			cover 0 0	vergrown (taller than inches) her (describe):
Any trees or undesired vegetation on crest?		T	X		T in			
Any depressions, cracks, animal burrows, ruts, or holes or	n crest?		X				X	
III. SLOPES – ABOVE THE WATER LEVEL		100000		e disease a service a service service	A Communication	TO ST Z	The second secon	
Forebay	Retention Basin			1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		CI	earwater Pond	
	Describe vegetation on the slope:	Describe vegetation on the slope:						
Sparse Good cover Overgrown (taller than 6-inches)	Sparse Good cover Overgrown 6-inches)						Overgrown (taller than 6-inches)	
Rip Rap Gravel Other (describe):	Rip Rap Gravel Other (des	cribe):		Rip Rap		Grav	rel 🗆	Other (describe):
Des	scription	Yes	No	Not Visible	Yes	No	Not Visible	Yes No Not Visible
2. Any depressions, cracks, animal burrows, ruts, or holes?			X	,	· /,		X	X
3. Above the water level, are there any cracks, evidence of	erosion, sloughs or indication of slope distress?		1				X	
IV. EXTERIOR SLOPES					736			Constant Co
Forebay	Retention Basin	Clearwater Pond						
/Describe vegetation on the slope:	Describe vegetation on the slope:	Describe vegetation on the slope:					in this is	
Sparse Good cover G-inches) Overgrown (taller than	(taller than Sparse Good cover Overgrown (taller than 6-inches)							
Rip Rap Gravel Other (describe):	Rip Rap Gravel Gravel Other (des	scribe):		Rip Ra	p L	J _{Gra}	avel	Other (describe):
2. Any areas of water-loving, (ex. cattails, grasses, etc.) ve	getation?		X			-		
3. Any depressions, bulges, holes, animal burrows, or erosi	ion on slope?		X			4		

4. Are there any cracks, sloughs or indication of slope distress?		
5. Do any wet areas indicate potential seepage through the dike?		
6. Are there any active seeps (flowing water) from the slope or toe of the dike? If yes, describe area, location, flow quantity, color etc.		
V. INLET AND OUTLET STRUCTURES		
1. What is the ESTIMATED free water level in the surface impoundment today?		
Forebay / Design Water Level: 100.5 ft gauge / 882.5 ft.	Retention Basin / Design Water Level: 99.5 ft gauge/880.5 ft.	Clearwater Pond
At Design Water Level Above Design Water Level Below Design Water Level	At Design Water Level Above Design Water Level Below Design Water Level	Design Water Level: 99 ft gauge / 880.0 ft. At Design Water Level Above Design Water Level Below Design Water Level
How would you describe the overall condition of the inlet structures?	How would you describe the overall condition of the inlet structures?	2. How would you describe the overall condition of the inlet structures?
Functioning Not Functional Deteriorated Normally Damaged Not Visible Other (describe):	Functioning Not Functional Deteriorated Normally Damaged Not Visible Other (describe):	Functioning Not Functional Deteriorated Normally Damaged Not Visible Other (describe):
How would you describe the overall condition of the outlet structures?	3. How would you describe the overall condition of the outlet structures?	How would you describe the overall condition of the outlet structures?
Functioning Not Functional Deteriorated	Functioning Not Functional Deteriorated Normally	Functioning Not Functional Deteriorated
Damaged Not Visible Other (describe):	□ Damaged □ Not Visible □ Other (describe):	Damaged Not Visible Other (describe):
If observable, describe any discharge from the outlet structure (turbidity, depth, etc.):	If observable, describe any discharge from the outlet structure (turbidity, depth, etc.):	If observable, describe any discharge from the outlet structure (turbidity, depth, etc.):
Is there evidence of damage, erosion, or obstruction around the INLET and OUTLET structures? If yes, describe:	Is there evidence of damage, erosion, or obstruction around the INLET and OUTLET structures? If yes, describe:	5. Is there evidence of damage, erosion, or obstruction around the INLET and OUTLET structures? If yes, describe:
☐Yes ☐Not Visible	Yes No Not Visible	Yes No Not Visible
VI. NOTES		
ITEM	Description/Location	
	RIA	
VII. PHOTOGRAPHS – HAS ENVIRONMENTAL SERVICES TAKEN PHOTOGRAPHS DURING THE QUARTER? (AT A MINIMUM ON A QUARTERLY BASIS AND WHENEVER NEEDED TO DOCUMENT ISSUES)		
At a minimum, photographs should be taken of the crest, interior and exterior slopes, and any other notable features.		